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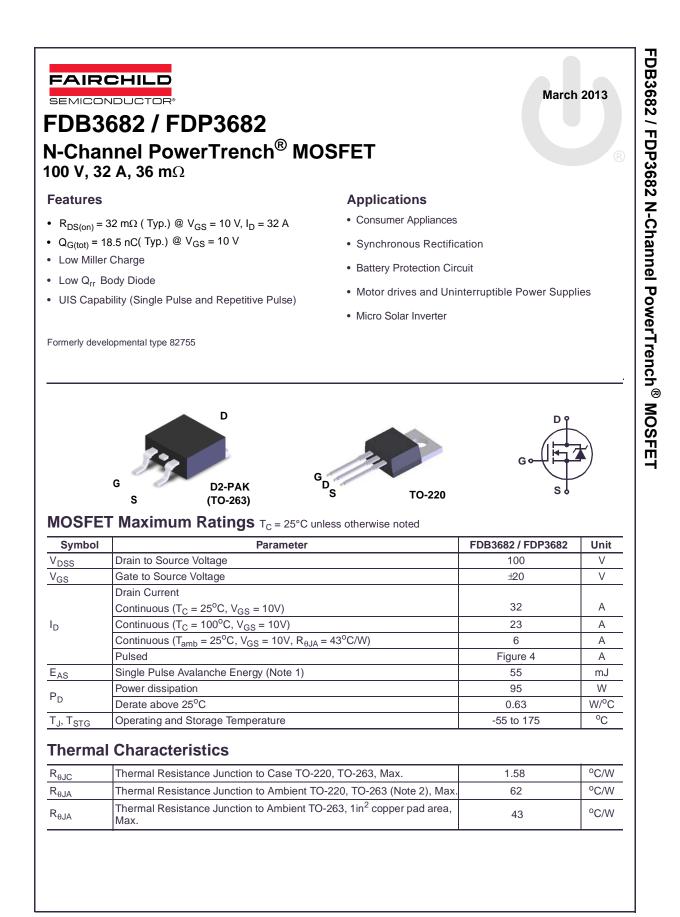


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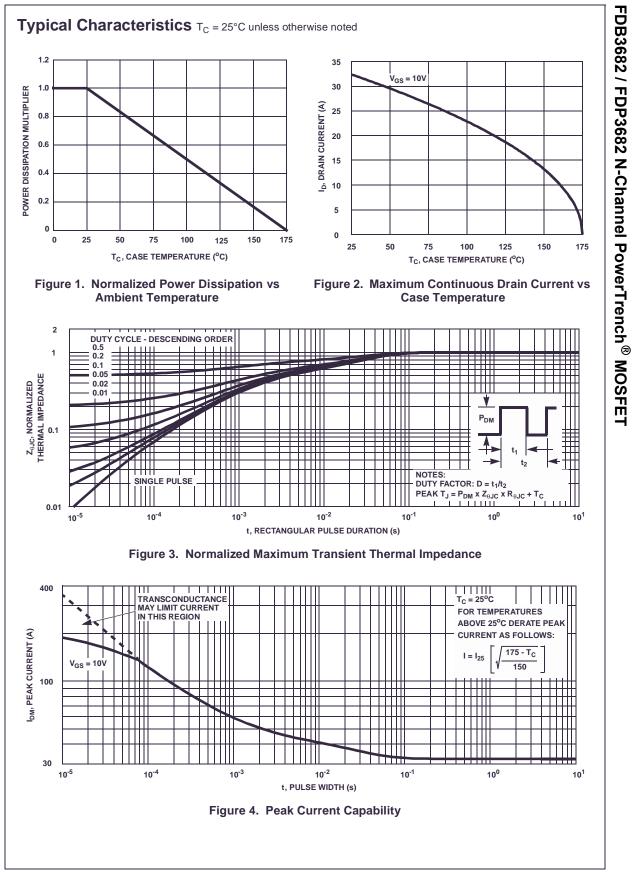
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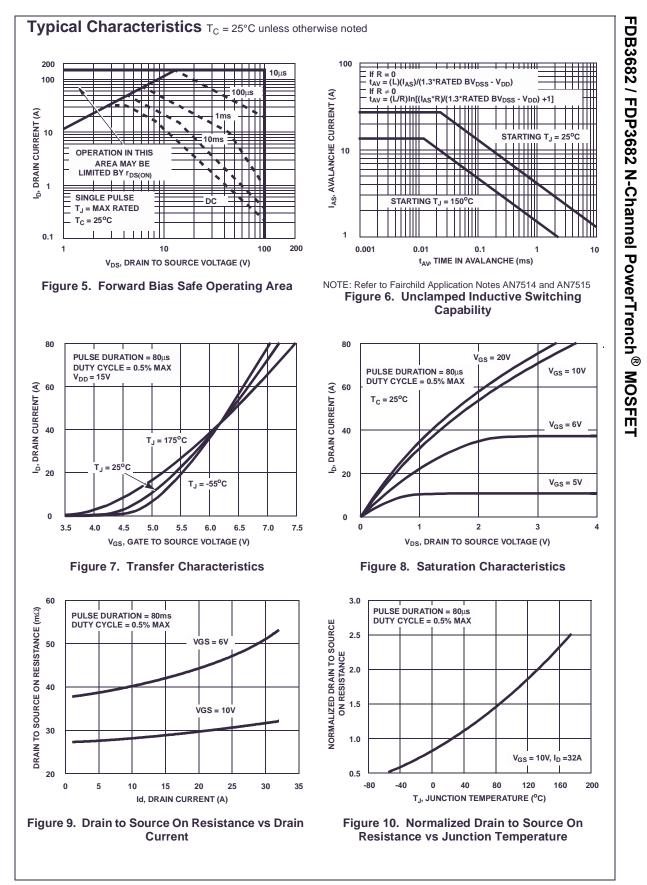
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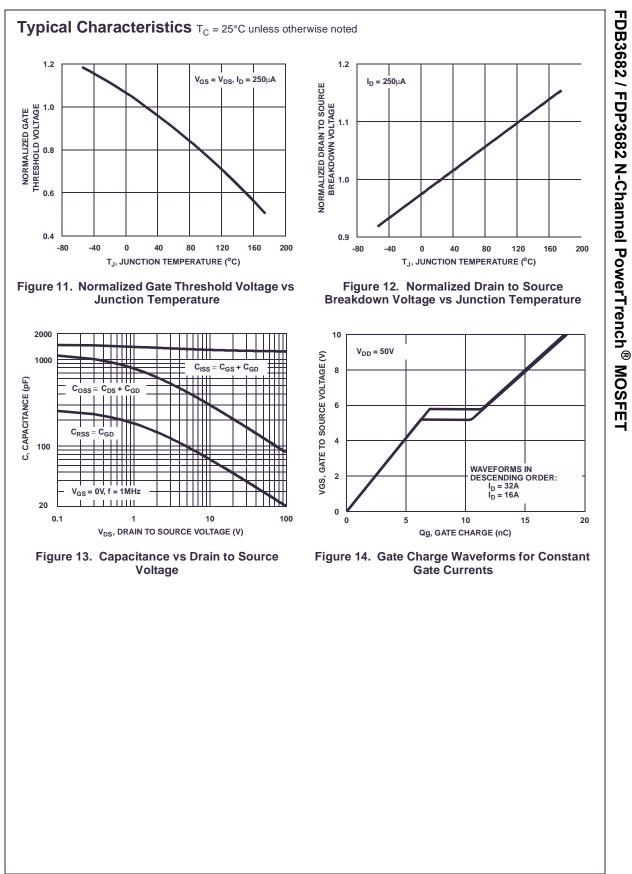
FDB3 FDP3		Device	Package	Reel Size	Tape Width 24mm		Quantity 800 units	
FDP3	682	FDB3682	TO-263	330mm				
	FDP3682 FDP3682		TO-220	Tube	N/A		50 units	
Electrica	al Chara	acteristics T _c = 25°C	unless otherwis	e noted				
Symbol		Parameter	Test	Conditions	Min	Тур	Мах	Unit
Off Chara	cteristics	6						
B _{VDSS}	Drain to S	ource Breakdown Voltage	I _D = 250μA,	$V_{GS} = 0V$	100	-	-	V
I _{DSS}	Zero Gate Voltage Drain Current		$V_{DS} = 80V$ $V_{GS} = 0V$	T _C = 150 ^o C	-	-	1 250	μA
I _{GSS}	Gate to Source Leakage Current		V _{GS} = ±20V	0	-	-	±100	nA
On Chara	1	•	- 63	I		1		
V _{GS(TH)}	Gate to S	ource Threshold Voltage	$V_{GS} = V_{DS},$	ь = 250uA	2	-	4	V
30(11)				$\frac{V_{GS} = V_{DS}, V_D = 200\mu V}{I_D = 32A, V_{GS} = 10V} - \frac{1}{1_D} = 16A, V_{GS} = 6V, - \frac{1}{1_D} = 16A, V_{GS} = 6V, - \frac{1}{1_D} = 16A, V_{GS} = 6V, - \frac{1}{1_D} = 16A, V_{GS} = 1000$		0.032	0.036	<u> </u>
r _{DS(ON)}	Drain to Source On Resistance					0.040	0.060	Ω
DS(UN)				$I_D = 10A, V_{GS} = 0V,$ $I_D = 32A, V_{GS} = 10V, T_C = 175^{\circ}C$		0.080	0.090	22
Dynamic	Characte	ristics	<u>1.0 0-0, 0</u>	,,	-	2.000		
C _{ISS}	Input Cap				-	1250	-	pF
C _{OSS}		apacitance	$V_{DS} = 25V,$	$V_{GS} = 0V,$	-	190	-	pF
C _{RSS}	-	ransfer Capacitance	f = 1MHz	-	-	45	-	pF
Q _{g(TOT)}		Charge at 10V	V _{GS} = 0V to	10\/	-	18.5	28	nC
	-	Gate Charge		2V V _{DD} = 50V	-	2.4	3.6	nC
Q _{g(TH)}		ource Gate Charge	VGS = 0V to	$V_{DD} = 50V$ $I_{D} = 32A$	-	6.5	-	nC
Q _{gs}		rge Threshold to Plateau		$I_{g} = 32A$ $I_{g} = 1.0mA$		4.1	-	nC
Q _{gs2}	_	rain "Miller" Charge				4.1	-	nC
Q _{gd}	1				-	4.0	_	no
	1	g Characteristics (V	_{GS} = 10V)			1	0.0	20
t _{ON}	Turn-On T				-	-	83	ns
t _{d(ON)}		elay Time		$V_{DD} = 50V, I_D = 32A$ $V_{GS} = 10V, R_{GS} = 16\Omega$		9	-	ns
t _r	Rise Time					46	-	ns
t _{d(OFF)}		elay Time	$v_{GS} = 10v,$			26	-	ns
t _f	Fall Time				-	32	-	ns
t _{OFF}	Turn-Off T				-	-	87	ns
Drain-Sou	Irce Dioc	le Characteristics		i		1	4.05) (
V _{SD}	Source to	Drain Diode Voltage	$I_{SD} = 32A$		-	-	1.25	V
	Povorao 5		$I_{SD} = 16A$	II /dt = 100 \/vc	-	-	1.0	
t _{rr}		Recovery Time		$II_{SD}/dt = 100A/\mu s$	-		55	ns
Q _{RR}	Reverse	Recovery Charge	$I_{SD} = 32A, C$	II _{SD} /dt = 100A/μs	-	-	90	nC

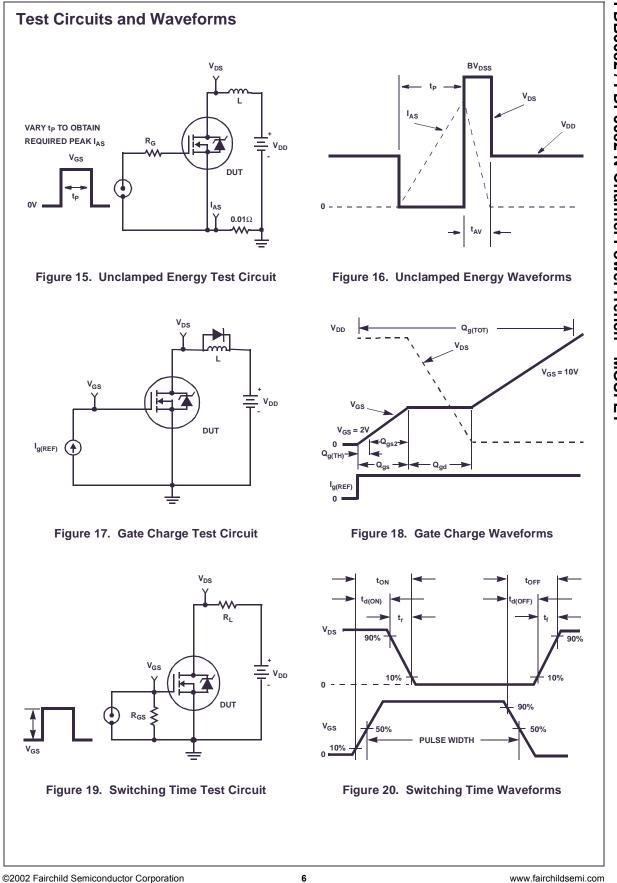


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FDB3682 / FDP3682 N-Channel PowerTrench[®] MOSFET

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Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature, T_{JM} , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation, P_{DM} , in an application. Therefore the application's ambient temperature, T_A (°C), and thermal resistance $R_{\theta JA}$ (°C/W) must be reviewed to ensure that T_{JM} is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}}$$
(EQ. 1)

In using surface mount devices such as the TO-263 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of P_{DM} is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- 2. The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- 6. For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

Fairchild provides thermal information to assist the designer's preliminary application evaluation. Figure 21 defines the $R_{\theta,JA}$ for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Fairchild device Spice thermal model or manually utilizing the normalized maximum transient thermal impedance curve.

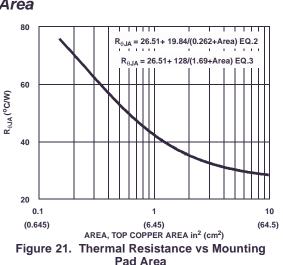
Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2 or 3. Equation 2 is used for copper area defined in inches square and equation 3 is for area in centimeter square. The area, in square inches or square centimeters is the top copper area including the gate and source pads.

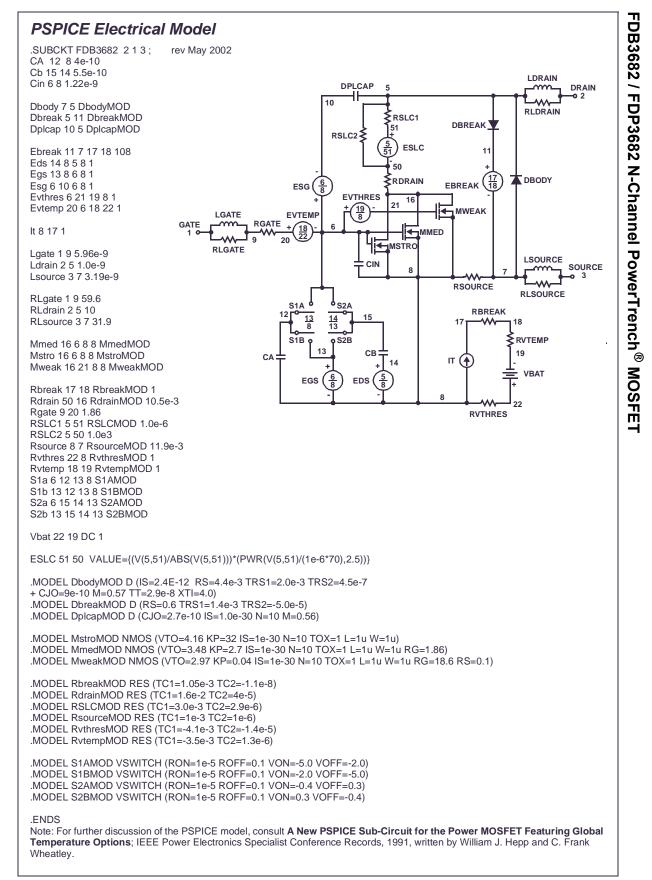
$$R_{\theta JA} = 26.51 + \frac{19.84}{(0.262 + Area)}$$
(EQ. 2)

Area in Inches Squared

$$R_{\theta JA} = 26.51 + \frac{128}{(1.69 + Area)}$$
(EQ. 3)

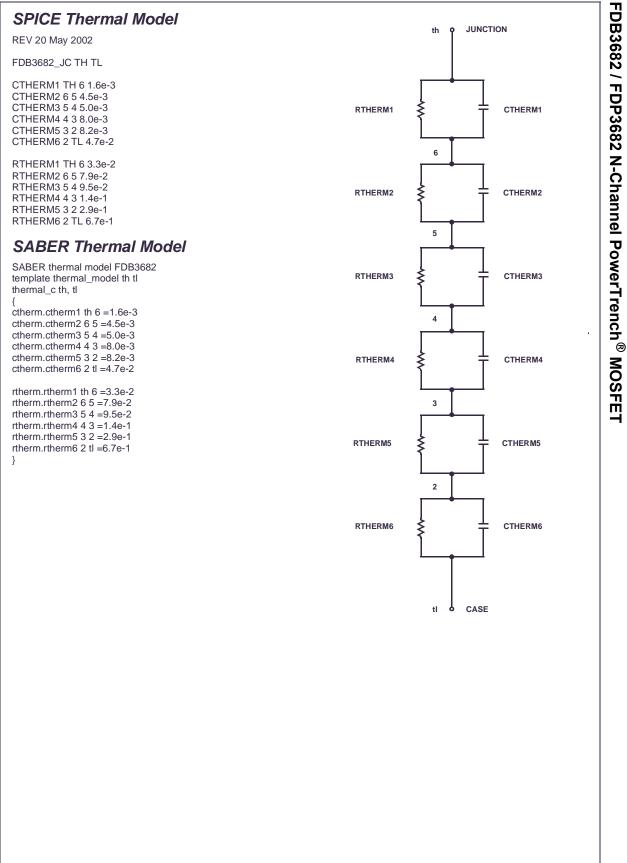
Area in Centimeters Squared



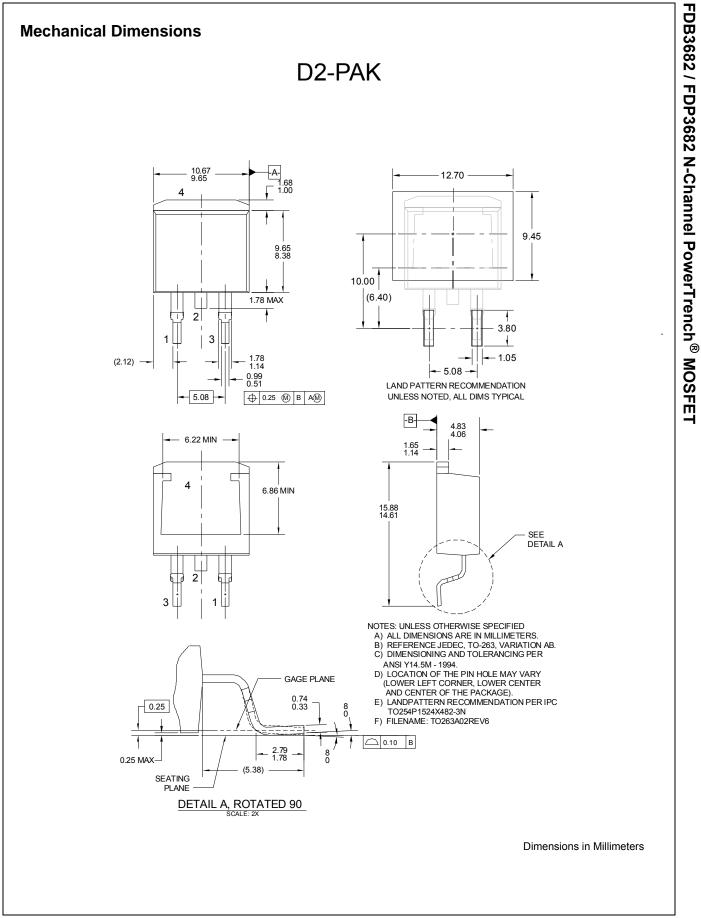


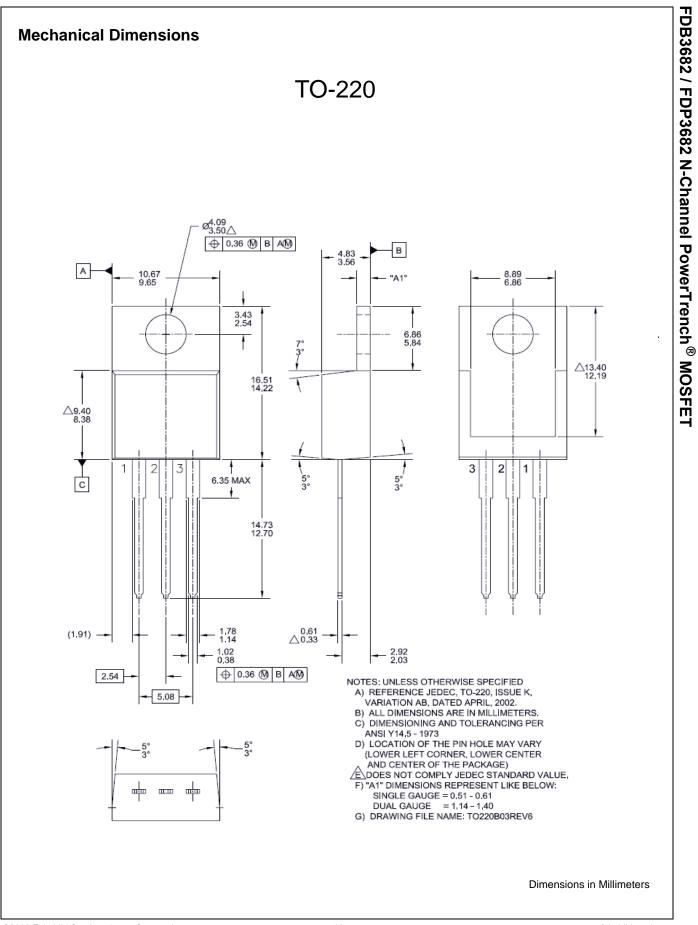
SABER Electrical Model REV May 2002 template FDB3682 n2,n1,n3 electrical n2,n1,n3 var i iscl dp..model dbodymod = (isl=2.4e-12,rs=4.4e-3,trs1=2.0e-3,trs2=4.5e-7,cjo=9e-10,m=0.57,tt=2.9e-8,xti=4.0) dp..model dbreakmod = (rs=0.6.trs1=1.4e-3.trs2=-5e-5)dp..model dplcapmod = (cjo=2.7e-10,isl=10e-30,nl=10,m=0.56) m..model mstrongmod = (type=_n,vto=4.16,kp=32,is=1e-30, tox=1) m..model mmedmod = $(type=_n, vto=3.48, kp=2.7, is=1e-30, tox=1)$ m..model mweakmod = (type=_n,vto=2.97,kp=0.04,is=1e-30, tox=1,rs=0.1) sw_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-5,voff=-2) I DRAIN sw_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-2,voff=-5) DPLCAP 5 DRAIN sw_vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-0.4,voff=0.3) -11 10 sw_vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=0.3,voff=-0.4) RLDRAIN c.ca n12 n8 = 4e-10 c.cb n15 n14 = 5.5e-10 51 RSLC2 ₹ c.cin n6 n8 = 1.22e-9 Ð ISCI dp.dbody n7 n5 = model=dbodymod DBREAK 50 dp.dbreak n5 n11 = model=dbreakmod RDRAIN 6 dp.dplcap n10 n5 = model=dplcapmod FSG 11 DBODY EVTHRES 16 spe.ebreak n11 n7 n17 n18 = 108 19 4 MWEAK I GATE EVTEMP spe.eds n14 n8 n5 n8 = 1 RGATE GATE \mathbf{m} spe.egs n13 n8 n6 n8 = 1 <u>18</u> 22 EBREAK 9 -20 spe.esg n6 n10 n6 n8 = 1 MSTRO RLGATE spe.evthres n6 n21 n19 n8 = 1 I SOURCE CIN spe.evtemp n20 n6 n18 n22 = 1 SOURCE 8 • \sim RSOURCE i.it n8 n17 = 1 RLSOURCE S1A S24 l.lgate n1 n9 = 5.96e-9 RBREAK <u>13</u> 8 <u>14</u> 13 I.ldrain n2 n5 = 1.0e-9 17 18 l.lsource n3 n7 = 3.19e-9 ≷RVTEMP o S2B S1B 13 СВ 19 res.rlgate n1 n9 = 59.6 CA IT (4) 14 res.rldrain n2 n5 = 10 VBAT res.rlsource n3 n7 = 31.9 6 EGS EDS 8 m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u 22 m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u RVTHRES m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u res.rbreak n17 n18 = 1, tc1=1.05e-3,tc2=-1.1e-8 res.rdrain n50 n16 = 10.5e-3, tc1=1.6e-2,tc2=4e-5 res.rgate n9 n20 = 1.86 res.rslc1 n5 n51 = 1.0e-6, tc1=3.0e-3,tc2=2.9e-6 res.rslc2 n5 n50 = 1.0e3 res.rsource n8 n7 = 11.9e-3, tc1=1e-3,tc2=1e-6 res.rvthres n22 n8 = 1, tc1=-4.1e-3,tc2=-1.4e-5 res.rvtemp n18 n19 = 1, tc1=-3.5e-3,tc2=1.3e-6 sw vcsp.s1a n6 n12 n13 n8 = model=s1amod sw_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw_vcsp.s2b n13 n15 n14 n13 = model=s2bmod v.vbat n22 n19 = dc=1 equations { i (n51->n50) +=iscl iscl: v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))*((abs(v(n5,n51)*1e6/70))** 2.5)) }

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