

8A and 12A Synchronous Step Down COT Regulator

General Description

The [XR76108](http://www.exar.com/XR76108) and [XR76112](http://www.exar.com/XR76112) are synchronous step-down regulators combining the controller, drivers, bootstrap diode and MOSFETs in a single package for point-of-load supplies. The XR76108 has a load current rating of 8A and the XR76112 has a load current rating of 12A. A wide 4.5V to 22V input voltage range allows for single supply operation from industry standard 5V, 12V and 19.6V rails.

With a proprietary emulated current mode Constant On-Time (COT) control scheme, the XR76108 and XR76112 provide extremely fast line and load transient response using ceramic output capacitors. They require no loop compensation, simplifying circuit implementation and reducing overall component count. The control loop also provides 0.25% load and 0.1% line regulation and maintains constant operating frequency. A selectable power saving mode, allows the user to operate in discontinuous mode (DCM) at light current loads thereby significantly increasing the converter efficiency.

A host of protection features, including over-current, over-temperature, short-circuit and UVLO, help achieve safe operation under abnormal operating conditions.

The XR76108/12 are available in a RoHS-compliant, green/halogen-free space-saving QFN 5x5mm package.

FEATURES

- 8A and 12A Capable Step Down Regulators
	- − 4.5V to 5.5V Low VIN Operation
	- − 4.5V to 22V Wide Single Input Voltage
	- − ≥0.6V Adjustable Output Voltage
- Controller, drivers, bootstrap diode and MOSFETs integrated in one package
- Proprietary Constant On-Time Control − No Loop Compensation Required
	- − Ceramic Output Cap. Stable operation
	- − Programmable 200ns-2µs On-Time
	- − Constant 200kHz-800kHz Freq.
	- − Selectable CCM or CCM/DCM Operation
- Precision Enable and Power-Good Flag
- Programmable Soft-start
- 5x5mm 30-pin QFN Package

APPLICATIONS

- Distributed Power Architecture
- Point-of-Load Converters
- Power Supply Modules
- FPGA, DSP, and Processor Supplies
- Base Stations, Switches/Routers, and Servers

Typical Application

Absolute Maximum Ratings

These are stress ratings only and functional operation of the device at these ratings or any other above those indicated in the operation sections of the specifications below is not implied. Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

Operating Ratings

Note 1: No external voltage applied

Note 2: SW pin's DC range is -1V, transient is -5V for less than 50ns

Note 3: Recommended

NOTES:

- 1. Refer to [www.exar.com/XR76108,](http://www.exar.com/XR76108) www.exar.com/XR76112 for most up-to-date Ordering Information.
- 2. Visit www.exar.com for additional information on Environmental Rating.

Electrical Characteristics

Specifications are for Operating Junction Temperature of $T_J = 25^{\circ}C$ only; limits applying over the full Operating Junction Temperature range are denoted by a "•". Typical values represent the most likely parametric norm at $T_J = 25^{\circ}$ C, and are provided for reference purposes only. Unless otherwise indicated, $V_{IN} = 12V$

XR76108 and XR76112

XR76108 and XR76112

Block Diagram

Figure 3: XR76108/12 Block Diagram

Pin Assignment

Figure 4: XR76108/12 Pin Assignment

Pin Description

Typical Performance Characteristics

All data taken at V_{IN}=12V, V_{OUT}=1.2V, f=600kHz, T_A=25°C, No Air flow, Forced CCM, unless otherwise specified. Schematic and BOM from Applications Circuit section of this datasheet.

REGULATION

Figure 9: XR76112 Frequency vs. Iout, Forced CCM Figure 10: VREF vs. temperature

Figure 5: XR76112 Load regulation, V_{IN} =12V Figure 6: XR76112 Line regulation, I_{OUT} =12A

Figure 7: XR76112 Vout ripple is 14mV at 12A Figure 8: XR76112 Vout ripple is 22mV at 0A, DCM

Typical Performance Characteristics

All data taken at V_{IN}=12V, V_{OUT}=1.2V, f=600kHz, T_A=25°C, No Air flow, Forced CCM, unless otherwise specified. Schematic and BOM from Applications Circuit section of this datasheet.

Figure 11: On-Time vs. temperature Figure 12: ILIM Vs. temperature

Figure 13: XR76108 load step, DCM/CCM, 0A-4A-0A Figure 14: XR76108 load step, Forced CCM, 4A-8-4A

Figure 15: XR76112 load step, DCM/CCM, 0A-6A-0A Figure 16: XR76112 load step, Forced CCM, 6A-12A-6A

Powerup

Figure 17: XR76112 Powerup, Forced CCM, I_{OUT}=0A Figure 18: XR76112 Powerup, Forced CCM, I_{OUT}=12A

Figure 21: XR76112 Enable turn on/turn off, 1.2V_{OUT}, 12A Figure 22: Typical loce versus RLIM

Figure 19: XR76112 Powerup, DCM/CCM, Iout=0A Figure 20: XR76112 Powerup, DCM/CCM, Iout=12A

Efficiency – XR76108/ XR76112

TAMBIENT=25°C, No Air flow, Inductor losses are included.

Figure 25: XR76108, 12V_{IN}, 600kHz Figure 26: XR76112, 12V_{IN}, 600kHz

Figure 27: XR76108, 22VIN, 400kHz, 3.3uH Figure 28: XR76112, 22VIN, 400kHz, 2.2uH

Figure 23: XR76108, 5VIN, 600kHz, 1uH Figure 24: XR76112, 5VIN, 600kHz, 0.56uH

Thermal Characteristics

No Air flow, f=600kHz

Figure 29: XR76108 Package Thermal Derating, 12VIN Figure 30: XR76108 Package Thermal Derating, 5VIN

Figure 31: XR76112 Package Thermal Derating, 12VIN Figure 32: XR76112 Package Thermal Derating, 5VIN

Detailed Operation

The XR76108/12 uses a synchronous step-down proprietary emulated current-mode Constant On-Time (COT) control scheme. The on-time, which is programmed via R_{ON} , is inversely proportional to V_{IN} and maintains a nearly constant frequency. The emulated current-mode control allows the use of ceramic output capacitors.

Each switching cycle begins with the high-side (switching) FET turning on for a preprogrammed time. At the end of the on-time, the high-side FET is turned off and the lowside (synchronous) FET is turned on for a preset minimum time (250ns nominal). This parameter is termed the Minimum Off-Time. After the minimum off-time the voltage at the feedback pin FB is compared to an internal voltage ramp at the feedback comparator. When V_{FB} drops below the ramp voltage, the high-side FET is turned on and the cycle repeats. This voltage ramp constitutes an emulated current ramp and allows for the use of ceramic capacitors, in addition to other capacitor types, for output filtering.

Enable/Mode

The EN/MODE pin accepts a tri-level signal that is used to control turn-on and turn-off. It also selects between two modes of operation: 'Forced CCM' and 'DCM/CCM'. If EN is pulled below 1.8V the regulator shuts down. A voltage between 2.0V and 2.8V selects the Forced CCM mode, which will run the converter in continuous conduction for all load currents. A voltage higher than 3.1V selects the DCM/CCM mode, which will run the converter in discontinuous conduction mode at light loads.

Selecting the Forced CCM Mode

In order to set the controller to operate in Forced CCM a voltage between 2.0V and 2.8V must be applied to EN/MODE. This can be achieved with an external control signal that meets the above voltage requirement. The $EN/MODE$ can be derived from V_{IN} where an external control is not available. If V_{IN} is well regulated, use a resistor divider and set the voltage to $2.45V$. If V_{IN} varies over a wide range, the circuit shown in figure 33 can be used to generate the required voltage.

Selecting the DCM/CCM Mode

In order to set the controller operation to DCM/CCM a voltage between 3.1V and 5.5V must be applied to EN/MODE pin and be sequenced with respect to V_{OUT} such that $2.0 \le V_{EN} \le 2.8V$ when V_{OUT} finishes softstart.

If an external 5V control signal is available use a low-pass RC and set the time constant to $RC = 5.5 \times t$ ss where tss is the softstart time. R should be in the 50k-100k range. Time t1 can be approximated from $t1 = 2.8 \times t$ ss. The timing circuit and diagram are shown in figure 34.

If an external 3.3V control signal is available, use a lowpass RC and set the time constant to RC=2.1×tss. R should be in the 50k-100k range. Time t1 can be approximated from t1=1.9×tss (figure 34).

Figure 33: Selecting Forced CCM by deriving EN/MODE from V_{IN}

EN/MODE input must be derived from V_{IN} in applications where an external control is not available. The timing circuit and diagram are shown in figure 35. Calculate the time constant from $RC = 4.7 \times$ tss. The value of R3 should be between 50k and 100k. t1 can be approximated from t1=2.7×tss. The R3 and C in figure 35 correspond to 2.8ms typical softstart of the application circuit.

Figure 35: Timing circuit and diagram for selecting DCM/CCM by deriving EN/MODE from VIN

Programming the On-Time

The on-time T_{ON} is programmed via resistor R_{ON} according to following equation:

$$
R_{ON} = \frac{V_{IN} \times [T_{ON} - (3 \times 10^{-8})]}{2.9 \times 10^{-10}}
$$

Where T_{ON} is calculated from:

$$
T_{ON} = \frac{V_{OUT}}{V_{IN} \times f \times Eff.}
$$

Where:

f is the desired switching frequency at nominal lout

Eff. is the converter efficiency corresponding to nominal IOUT

Substituting for T_{ON} in the first equation we get:

$$
R_{ON} = \frac{\left(\frac{V_{OUT}}{f \times Eff}\right) - [(3 \times 10^{-8}) \times V_{IN}]}{(2.9 \times 10^{-10})}
$$

At V_{IN} =12V, f=600kHz, I_{OUT} =8A and using the efficiency numbers from figure 25 we get the following R_{ON} for XR76108:

R_{ON} (kΩ)
29.3
19.4
14.5
10.4
8.67
6.87
5.68

Figure 36: XR76108 Ron for common output voltages, V_{IN} =12V, $I_{OUT}=8A$, $f=600kHz$

Over-Current Protection (OCP)

If the load current exceeds the programmed over-current locp for four consecutive switching cycles, then the regulator enters the hiccup mode of operation. In hiccup mode the MOSFET gates are turned off for 110ms (hiccup timeout). Following the hiccup timeout a soft-start is attempted. If OCP persists, hiccup timeout will repeat. The regulator will remain in hiccup mode until load current is reduced below the programmed locp. In order to program over-current protection use the following equation:

$$
R_{ILIM} = \frac{(I_{OCP} \times R_{DSON}) + 8mV}{I_{LIM}}
$$

where:

RLIM is resistor value for programming locp

I_{OCP} is the over-current value to be programmed

 R_{DSON} =10m Ω (XR76108)

 $R_{DSON}=9mΩ(XR76112)$

8mV is the OCP comparator offset

 I_{LIM} is the internal current that generates the necessary OCP comparator threshold (45µA)

Note that ILIM has a positive temperature coefficient of 0.4%/°C. This is meant to approximately match and compensate for positive temperature coefficient of the synchronous FET's RDSON.

The above equation is for worst-case analysis and safeguards against premature OCP. Actual value of locp, for a given RLIM, will be higher than that predicted by the above equation. Typical locp versus RLIM is shown in Figure 22.

Short-Circuit Protection (SCP)

If the output voltage drops below 60% of its programmed value, the regulator will enter hiccup mode. Hiccup mode will persist until the short-circuit is removed. The SCP circuit becomes active after PGOOD asserts high.

Over-Temperature Protection (OTP)

OTP triggers at a nominal controller temperature of 150°C. The gates of the switching FET and the synchronous FET are turned off. When controller temperature cools down to 135°C, soft-start is initiated and operation resumes.

Programming the Output Voltage

Use an external voltage divider as shown in Figure 1 to program the output voltage V_{OUT} .

$$
R1 = R2 \times \left(\frac{V_{OUT}}{0.6} - 1\right)
$$

The recommended value for R2 is 2kΩ.

Programming the Soft-start

Place a capacitor Css between the SS and GND pins to program the soft-start. In order to program a soft-start time of T_{SS} , calculate the required capacitance C_{SS} from the following equation:

$$
C_{SS} = T_{SS} \times \frac{10uA}{0.6V}
$$

Feed-Forward Capacitor CFF

The voltage divider R1-R2 attenuates the output voltage ripple ($V_{OUT,RIPPLE}$) that is fed back to controller's FB pin. The steady-state voltage ripple at FB (VFB,RIPPLE) must not exceed 50mV in order for the controller to function correctly. If V_{FB,RIPPLE} is larger than 50mV, a CFF should not be used. Cout should be increased as necessary in order to keep the VFB,RIPPLE below 50mV.

It is recommended to use a feed-forward capacitor (C_{FF}) if output voltage ripple ($V_{\text{OUT,RIPPLE}}$) is less than 50mV. C_{FF} provides a low-impedance/high-frequency path for the $V_{OUT,RIPPLE}$ to be transmitted to FB. It also helps get an optimum transient load response. Calculate C_{FF} from:

$$
C_{FF} = \frac{1}{2 \times \pi \times f \times 0.1 \times R1}
$$

A load step test should be performed and if necessary C_{FF} can be adjusted in order to get a critically damped transient load response.

Feed-Forward Resistor RFF

Fast Turn on and turn off of power FETs gives rise to switching noise that may be coupled to the feedback pin. Excessive switching noise at FB will result in poor load regulation. A resistor R_{FF}, in series with C_{FF} helps decouple noise and restore good load regulation. Maximum value of R_{FF} should not exceed $0.02 \times R1$.

Thermal Design

Proper thermal design is critical in controlling device temperatures and in achieving robust designs. There are a number of factors that affect the thermal performance. One key factor is the temperature rise of the devices in the package, which is a function of the thermal resistances of the devices inside the package and the power being dissipated.

The thermal resistances of the XR76108/12 are specified in the "Operating Ratings" section of this datasheet. The JEDEC θJA thermal resistance provided is based on tests that comply with the JESD51-2A "Integrated Circuit Thermal Test Method Environmental Conditions – Natural Convection" standard. JESD51-xx are a group of standards whose intent is to provide comparative data based on a standard test condition which includes a defined board construction. Since the actual board design in the final application will be different from the board defined in the standard, the thermal resistances in the final design may be different from those shown.

The package thermal derating curves for the XR76108 are shown in Figures 29 and 30. These correspond to input voltage of 12V and 5V respectively. The package thermal derating curves for the XR76112 are shown in Figures 31 and 32.

Operation at VIN<6V

As V_{IN} falls below approximately 5V, the V_{cc} regulator will start to operate in dropout. This means it is no longer regulating the output of V_{cc} . V_{cc} is designed with a UVLO function to ensure all internal circuitry has sufficient voltage to operate to meet datasheet specifications and properly drive the internal MOSFETs. The UVLO is set to allow the chip to start operating once V_{CC} reaches 4.25V and will disable the chip if the voltage falls below 4.00V.

When V_{IN} is 4.5V and the part is not switching, the output of the V_{cc} regulator will be close to V_{IN} and be high enough to ensure it is above the V_{cc} UVLO. Although once switching starts the output of V_{CC} may fall as low as 4.3V, the UVLO shutdown threshold is guaranteed to be less than 4.25V.

Applications Circuit

Figure 37: XR76112 Application circuit schematic

Figure 37: XR76108 Application circuit schematic

Mechanical Dimensions

Revision:

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Revision History

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