

### **600 nA, Non-Unity Gain Rail-to-Rail Input/Output Op Amps**

#### **Features:**

- Low Quiescent Current: 600 nA/amplifier (typ.)
- Gain Bandwidth Product: 100 kHz (typ.)
- Stable for gains of 10 V/V or higher
- Rail-to-Rail Input/Output
- Wide Supply Voltage Range: 1.4V to 5.5V
- Available in Single, Dual, and Quad
- Chip Select  $(\overline{CS})$  with MCP6143
- Available in 5-lead and 6-lead SOT-23 Packages
- Temperature Ranges:
	- Industrial: -40°C to +85°C
	- Extended: -40°C to +125°C

#### **Applications:**

- Toll Booth Tags
- Wearable Products
- Temperature Measurement
- Battery Powered

#### **Available Tools:**

- SPICE Macro Models (at www.microchip.com)
- FilterLab™ Software (at www.microchip.com)

#### **Related Devices:**

• MCP6041/2/3/4: Unity Gain Stable Op Amps

#### **Typical Application**



#### **Description:**

The MCP6141/2/3/4 family of non-unity gain stable operational amplifiers (op amps) from Microchip Technology Inc. operate with a single supply voltage as low as 1.4V, while drawing less than 1 μA (max.) of quiescent current per amplifier. These devices are also designed to support rail-to-rail input and output operation. This combination of features supports battery-powered and portable applications.

The MCP6141/2/3/4 amplifiers have a gain bandwidth product of 100 kHz (typ.) and are stable for gains of 10 V/V or higher. These specifications make these op amps appropriate for battery powered applications where a higher frequency response from the amplifier is required.

The MCP6141/2/3/4 family operational amplifiers are offered in single (MCP6141), single with Chip Select  $(\overline{CS})$  (MCP6143), dual (MCP6142) and quad (MCP6144) configurations. The MCP6141 device is available in the 5-lead SOT-23 package, and the MCP6143 device is available in the 6-lead SOT-23 package.

#### **Package Types**



#### <span id="page-1-0"></span>**1.0 ELECTRICAL CHARACTERISTICS**

#### **Absolute Maximum Ratings †**



**† Notice:** Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at those or any other conditions above those indicated in the operational listings of this specification is not implied. Exposure to maximum rating conditions for extended periods may affect device reliability.

#### **DC ELECTRICAL CHARACTERISTICS**





#### **AC ELECTRICAL CHARACTERISTICS**



### **MCP6143 CHIP SELECT (CS) ELECTRICAL CHARACTERISTICS**





<span id="page-2-0"></span>*FIGURE 1-1: Chip Select (CS) Timing Diagram (MCP6143 only).*

#### **TEMPERATURE CHARACTERISTICS**



<span id="page-3-0"></span>**Note 1:** The MCP6141/2/3/4 family of Industrial Temperature op amps operates over this extended range, but with reduced performance. In any case, the internal Junction Temperature  $(T_J)$  should not exceed the Absolute Maximum specification of +150°C.

#### <span id="page-4-0"></span>**2.0 TYPICAL PERFORMANCE CURVES**

**Note:** The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only. The performance characteristics listed herein are not tested or guaranteed. In some graphs or tables, the data presented may be outside the specified operating range (e.g., outside specified power supply range) and therefore outside the warranted range.

**Note:** Unless otherwise indicated,  $T_A = 25^{\circ}C$ ,  $V_{DD} = +1.4V$  to +5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/2$ ,  $R_L = 1 M\Omega$  to  $V_{DD}/2$ ,  $V_{\text{OUT}} \approx V_{\text{DD}}/2$ , and  $C_{\text{L}} = 60 \text{ pF}$ .



*FIGURE 2-1: Input Offset Voltage at*   $V_{DD} = 1.4V$ .



*FIGURE 2-2: Input Offset Voltage Drift at*   $V_{DD} = 1.4V$ .



*FIGURE 2-3: Input Offset Voltage vs. Common Mode Input Voltage at V<sub>DD</sub> = 1.4V.* 



*FIGURE 2-4: Input Offset Voltage at* 









*FIGURE 2-5: Input Offset Voltage Drift at*   $V_{DD} = 5.5V$ .



*FIGURE 2-6: Input Offset Voltage vs. Common Mode Input Voltage at V<sub>DD</sub> = 5.5V.* 

**Note:** Unless otherwise indicated,  $T_A = 25^{\circ}$ C,  $V_{DD} = +1.4V$  to +5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/2$ ,  $R_L = 1 M\Omega$  to  $V_{DD}/2$ ,  $V_{OUT} \approx V_{DD}/2$ , and  $C_L = 60$  pF.







*FIGURE 2-8: Input Noise Voltage Density vs. Frequency.*



*FIGURE 2-9: CMRR, PSRR vs. Frequency.*



<span id="page-5-0"></span>*FIGURE 2-10: The MCP6141/2/3/4 family shows no phase reversal.*



*FIGURE 2-11: Input Noise Voltage Density vs. Common Mode Input Voltage.*



*FIGURE 2-12: CMRR, PSRR vs. Ambient Temperature.*

**Note:** Unless otherwise indicated,  $T_A = 25^{\circ}$ C,  $V_{DD} = +1.4V$  to +5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/2$ ,  $R_L = 1 M\Omega$  to  $V_{DD}/2$ ,  $V_{\text{OUT}} \approx V_{\text{DD}}/2$ , and  $C_1 = 60 \text{ pF}$ .



*FIGURE 2-13: Input Bias, Offset Currents vs. Ambient Temperature.*



*FIGURE 2-14: Open-Loop Gain, Phase vs. Frequency.*



*FIGURE 2-15: DC Open-Loop Gain vs. Power Supply Voltage.*



*FIGURE 2-16: Input Bias, Offset Currents vs. Common Mode Input Voltage.*



*FIGURE 2-17: DC Open-Loop Gain vs. Load Resistance.*



*FIGURE 2-18: DC Open-Loop Gain vs. Output Voltage Headroom.*

**Note:** Unless otherwise indicated,  $T_A = 25^{\circ}$ C, V<sub>DD</sub> = +1.4V to +5.5V, V<sub>SS</sub> = GND, V<sub>CM</sub> = V<sub>DD</sub>/2, R<sub>L</sub> = 1 MΩ to V<sub>DD</sub>/2,  $V_{\text{OUT}} \approx V_{\text{DD}}/2$ , and  $C_1 = 60 \text{ pF}$ .



*FIGURE 2-19: Channel-to-Channel Separation vs. Frequency (MCP6142 and MCP6144 only).*



*FIGURE 2-20: Gain Bandwidth Product, Phase Margin vs. Ambient Temperature at*   $V_{DD} = 1.4V$ .



*FIGURE 2-21: Quiescent Current vs. Power Supply Voltage.*



*FIGURE 2-22: Gain Bandwidth Product, Phase Margin vs. Common Mode Input Voltage.*







*FIGURE 2-24: Output Short Circuit Current vs. Power Supply Voltage.*

**Note:** Unless otherwise indicated,  $T_A = 25^{\circ}$ C,  $V_{DD} = +1.4V$  to +5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/2$ ,  $R_L = 1 M\Omega$  to  $V_{DD}/2$ ,  $V_{\text{OUT}} \approx V_{\text{DD}}/2$ , and  $C_1 = 60 \text{ pF}$ .



*FIGURE 2-25: Output Voltage Headroom vs. Output Current Magnitude.*



*FIGURE 2-26: Slew Rate vs. Ambient Temperature.*



*Pulse Response.*

*FIGURE 2-27: Small Signal Non-inverting* 







*FIGURE 2-29: Maximum Output Voltage Swing vs. Frequency.*



*Response.*

*FIGURE 2-30: Small Signal Inverting Pulse* 

**Note:** Unless otherwise indicated,  $T_A = 25^{\circ}$ C,  $V_{DD} = +1.4V$  to +5.5V,  $V_{SS} = GND$ ,  $V_{CM} = V_{DD}/2$ ,  $R_L = 1 M\Omega$  to  $V_{DD}/2$ ,  $V_{OUT} \approx V_{DD}/2$ , and  $C_L = 60$  pF.



*FIGURE 2-31: Large Signal Non-inverting Pulse Response.*



*FIGURE 2-32: Chip Select (CS) to Amplifier Output Response Time (MCP6143 only).*



*FIGURE 2-33: Large Signal Inverting Pulse Response.*



*FIGURE 2-34: Internal Chip Select (CS) Hysteresis (MCP6143 only).*

#### <span id="page-10-1"></span>**3.0 PIN DESCRIPTIONS**

Descriptions of the pins are listed in [Table 3-1](#page-10-0).

<b>MCP6141</b> (PDIP, SOIC, MSOP)	<b>MCP6141</b> (SOT-23-5)	<b>MCP6142</b>	<b>MCP6143</b> (PDIP, SOIC, MSOP)	<b>MCP6143</b> $(SOT-23-6)$	<b>MCP6144</b>	Symbol	<b>Description</b>
6	1	1	6	1	1	VOUT, VOUTA	Analog Output (op amp A)
$\overline{2}$	4	2	$\overline{2}$	4	2	$V_{IN}$ , $V_{INA}$ –	Inverting Input (op amp A)
3	3	3	3	3	3	$V_{IN}+$ , $V_{INA}+$	Non-inverting Input (op amp A)
$\overline{7}$	5	8	$\overline{7}$	6	$\overline{4}$	$V_{DD}$	Positive Power Supply
		5			5	$V_{INB}$ +	Non-inverting Input (op amp B)
		6			6	$V_{INB}$	Inverting Input (op amp B)
		$\overline{7}$			7	<b>VOUTB</b>	Analog Output (op amp B)
					8	VOUTC	Analog Output (op amp C)
					9	$V_{INC}$	Inverting Input (op amp C)
					10	$V_{INC}+$	Non-inverting Input (op amp C)
4	$\overline{2}$	$\overline{4}$	4	2	11	$V_{SS}$	<b>Negative Power Supply</b>
					12	$VIND +$	Non-inverting Input (op amp D)
					13	V <sub>IND</sub>	Inverting Input (op amp D)
					14	VOUTD	Analog Output (op amp D)
			8	5		$\overline{\text{cs}}$	Chip Select
1, 5, 8			1, 5			<b>NC</b>	No Internal Connection

<span id="page-10-0"></span>**TABLE 3-1: PIN FUNCTION TABLE**

#### **3.1 Analog Outputs**

The output pins are low-impedance voltage sources.

#### **3.2 Analog Inputs**

The non-inverting and inverting inputs are high-impedance CMOS inputs with low bias currents.

#### **3.3 CS Digital Input**

This is a CMOS, Schmitt-triggered input that places the part into a low-power mode of operation.

#### **3.4** Power Supply (V<sub>SS</sub> and V<sub>DD</sub>)

The positive power supply pin  $(V_{DD})$  is 1.4V to 5.5V higher than the negative power supply pin  $(V_{SS})$ . For normal operation, the other pins are at voltages between  $V_{SS}$  and  $V_{DD}$ .

Typically, these parts are used in a single (positive) supply configuration. In this case,  $V_{SS}$  is connected to ground and  $V_{DD}$  is connected to the supply.  $V_{DD}$  will need a local bypass capacitor (typically 0.01 μF to 0.1 μF) within 2 mm of the  $V_{DD}$  pin. These can share a bulk capacitor with nearby analog parts (within 100 mm), but it is not required.

#### <span id="page-11-1"></span>**4.0 APPLICATIONS INFORMATION**

The MCP6141/2/3/4 family of op amps is manufactured using Microchip's state-of-the-art CMOS process These op amps are stable for gains of 10 V/V and higher. They are suitable for a wide range of general purpose, low-power applications.

See Microchip's related MCP6041/2/3/4 family of op amps for applications needing unity gain stability.

#### **4.1 Rail-to-Rail Inputs**

The MCP6141/2/3/4 op amps are designed to prevent phase reversal when the input pins exceed the supply voltages. [Figure 2-10](#page-5-0) shows the input voltage exceeding the supply voltage without any phase reversal.

The input stage of the MCP6141/2/3/4 op amps uses two differential CMOS input stages in parallel. One operates at low Common mode input voltage  $(V_{CM})$ , while the other operates at high  $V_{CM}$ . With this topology, the device operates with  $V_{CM}$  tp to 0.3V above  $V_{DD}$ and 0.3V below  $V_{SS}$ . The input offset voltage ( $V_{OS}$ ) is measured at  $V_{CM} = V_{SS} - 0.3V$  and  $V_{DD} + 0.3V$  to ensure proper operation.

Input voltages that exceed the Absolute Maximum Voltage Range ( $V_{SS}$  – 0.3V to  $V_{DD}$  + 0.3V) can cause excessive current to flow into or out of the input pins. Current beyond  $\pm 2$  mA can cause reliability problems. Applications that exceed this rating must be externally limited with a resistor, as shown in [Figure 4-1](#page-11-0).



<span id="page-11-0"></span>*FIGURE 4-1: Input Current-Limiting Resistor (RIN).*

#### **4.2 Rail-to-Rail Output**

There are two specifications that describe the output swing capability of the MCP6141/2/3/4 family of op amps. The first specification (Maximum Output Voltage Swing) defines the absolute maximum swing that can be achieved under the specified load condition. Thus, the output voltage swings to within 10 mV of either supply rail with a 50 kΩ load to  $V_{DD}/2$ . [Figure 2-10](#page-5-0) shows how the output voltage is limited when the input goes beyond the linear region of operation.

The second specification that describes the output swing capability of these amplifiers is the Linear Output Voltage Range. This specification defines the maximum output swing that can be achieved while the amplifier still operates in its linear region. To verify linear operation in this range, the large signal DC Open-Loop Gain  $(A<sub>OL</sub>)$  is measured at points inside the supply rails. The measurement must meet the specified  $A_{\Omega}$  condition in the specification table.

#### **4.3 Output Loads and Battery Life**

The MCP6141/2/3/4 op amp family has outstanding quiescent current, which supports battery-powered applications. There is minimal quiescent current glitching when Chip Select (CS) is raised or lowered. This prevents excessive current draw, and reduced battery life, when the part is turned off or on.

Heavy resistive loads at the output can cause excessive battery drain. Driving a DC voltage of 2.5V across a 100 kΩ load resistor will cause the supply current to increase by 25 μA, depleting the battery 43 times as fast as  $I<sub>Q</sub>$  (0.6  $\mu$ A, typ.) alone.

High frequency signals (fast edge rate) across capacitive loads will also significantly increase supply current. For instance, a  $0.1 \mu$ F capacitor at the output presents an AC impedance of 15.9 kΩ (1/2πfC) to a 100 Hz sinewave. It can be shown that the average power drawn from the battery by a 5.0  $V_{p-p}$  sinewave (1.77  $V_{rms}$ ), under these conditions, is

**EQUATION 4-1:**

$$
P_{\text{Supply}} = (V_{DD} - V_{SS}) (I_Q + V_{L(p-p)} f C_L)
$$
  
= (5V)(0.6 \mu A + 5.0V\_{p-p} \cdot 100Hz \cdot 0.1 \mu F)  
= 3.0 \mu W + 50 \mu W

This will drain the battery 18 times as fast as  $I<sub>O</sub>$  alone.

#### **4.4 Stability**

#### 4.4.1 NOISE GAIN

The MCP6141/2/3/4 op amp family is designed to give high bandwidth and slew rate for circuits with high noise gain  $(G_N)$  or signal gain. Low gain applications should be realized using the MCP6041/2/3/4 op amp family; this simplifies design and implementation issues.

Noise gain is defined to be the gain from a voltage source at the non-inverting input to the output when all other voltage sources are zeroed (shorted out). Noise gain is independent of signal gain and depends only on components in the feedback loop. The amplifier circuits in [Figure 4-2](#page-12-0) and [Figure 4-3](#page-12-1) have their noise gain calculated as follows:

#### **EQUATION 4-2:**

$$
G_N = 1 + \frac{R_F}{R_G} \ge 10 \ V/V
$$

In order for the amplifiers to be stable, the noise gain should meet the specified minimum noise gain. Note that a noise gain of  $G_N = +10$  V/V corresponds to a non-inverting signal gain of  $G = +10$  V/V, or to an inverting signal gain of  $G = -9$  V/V.



<span id="page-12-0"></span>*FIGURE 4-2: Noise Gain for Non-inverting Gain Configuration.*



<span id="page-12-1"></span>*FIGURE 4-3: Noise Gain for Inverting Gain Configuration.*

[Figure 4-4](#page-12-2) shows a unity gain buffer and Miller integrator that are unstable when used with the MCP6141/2/3/4 family. Note that the capacitor makes the integrator circuit reach unity gain at high frequencies, which makes these op amps unstable.



<span id="page-12-2"></span>*FIGURE 4-4: Typical Unstable Circuits for the MCP6141/2/3/4 Family.*

#### 4.4.2 CAPACITIVE LOADS

Driving large capacitive loads can cause stability problems for voltage feedback op amps. As the load capacitance increases, the feedback loop's phase margin decreases and the closed-loop bandwidth is reduced. This produces gain peaking in the frequency response, with overshoot and ringing in the step response. A unity gain buffer  $(G = +1)$  is the most sensitive to capacitive loads, though all gains show the same general behavior.

When driving large capacitive loads with these op amps (e.g.,  $> 60$  pF when  $G = +10$ ), a small series resistor at the output ( $R_{ISO}$  in [Figure 4-5](#page-12-3)) improves the feedback loop's phase margin (stability) by making the output load resistive at higher frequencies. The bandwidth will be generally lower than the bandwidth with no capacitive load.



<span id="page-12-3"></span>*FIGURE 4-5: Output Resistor, R<sub>ISO</sub> stabilizes large capacitive loads.*

[Figure 4-6](#page-12-4) gives recommended  $R_{\text{ISO}}$  values for different capacitive loads and gains. The x-axis is the normalized load capacitance  $(C_L/G_N)$ , where  $G_N$  is the circuit's noise gain. For non-inverting gains,  $G_N$  and the Signal Gain are equal. For inverting gains,  $G_N$  is 1+|Signal Gain| (e.g., -9 V/V gives  $G_N$  = +10 V/V).



<span id="page-12-4"></span>*FIGURE 4-6: Recommended RISO Values for Capacitive Loads.*

After selecting  $R_{ISO}$  for your circuit, double check the resulting frequency response peaking and step response overshoot. Modify  $R_{ISO}$ 's value until the response is reasonable. Bench evaluation and simulations with the MCP6141/2/3/4 SPICE macro model are helpful.

#### **4.5 MCP6143 Chip Select (CS)**

The MCP6143 is a single op amp with Chip Select  $(\overline{CS})$ . When  $\overline{CS}$  is pulled high, the supply current drops to 50 nA (typ.) and flows through the  $\overline{\text{CS}}$  pin to  $\text{V}_{\text{SS}}$ . When this happens, the amplifier output is put into a high impedance state. By pulling  $\overline{CS}$  low, the amplifier is enabled. If the  $\overline{CS}$  pin is left floating, the amplifier may not operate properly. [Figure 1-1](#page-2-0) shows the output voltage and supply current response to a  $\overline{\text{CS}}$  pulse.

#### **4.6 Supply Bypass**

With this family of operational amplifiers, the power supply pin  $(V_{DD}$  for single supply) should have a local bypass capacitor (i.e.,  $0.01 \mu$ F to  $0.1 \mu$ F) within 2 mm for good high frequency performance. It can use a bulk capacitor (i.e., 1 μF or larger) within 100 mm to provide large, slow currents. This bulk capacitor is not required for most applications and can be shared with other nearby analog parts.

#### **4.7 Unused Op Amps**

An unused op amp in a quad package (MCP6144) should be configured as shown in [Figure 4-7.](#page-13-0) These circuits prevent the output from toggling and causing crosstalk. Circuits A and B are set near the minimum noise gain. Circuit A can use any reference voltage between the supplies, provides a buffered DC voltage, and minimizes the supply current draw of the unused op amp. Circuit B may draw a little more supply current for the unused op amp. Circuit C uses the minimum number of components and operates as a comparator; it may draw more current than either Circuit A or B.



<span id="page-13-0"></span>*FIGURE 4-7: Unused Op Amps.*

#### **4.8 PCB Surface Leakage**

In applications where low input bias current is critical, printed circuit board (PCB) surface leakage effects need to be considered. Surface leakage is caused by humidity, dust or other contamination on the board. Under low humidity conditions, a typical resistance between nearby traces is 10<sup>12</sup> $\Omega$ . A 5V difference would cause 5 pA of current to flow, which is greater than the MCP6141/2/3/4 family's bias current at 25°C (1 pA, typ.).

The easiest way to reduce surface leakage is to use a guard ring around sensitive pins (or traces). The guard ring is biased at the same voltage as the sensitive pin. An example of this type of layout is shown in [Figure 4-8.](#page-13-1)



#### <span id="page-13-1"></span>*FIGURE 4-8: Example Guard Ring Layout for Inverting Gain.*

- 1. Non-inverting Gain and Unity Gain Buffer:
	- a) Connect the non-inverting pin  $(V_{IN}+)$  to the input with a wire that does not touch the PCB surface.
	- b) Connect the guard ring to the inverting input pin  $(V_{1N}-)$ . This biases the guard ring to the Common mode input voltage.
- 2. Inverting Gain and Trans-impedance Gain (convert current to voltage, such as photo detectors) amplifiers:
	- a) Connect the guard ring to the non-inverting input pin  $(V_{IN}+)$ . This biases the guard ring to the same reference voltage as the op amp (e.g.,  $V_{DD}/2$  or ground).
	- b) Connect the inverting pin  $(V_{1N}-)$  to the input with a wire that does not touch the PCB surface.

#### **4.9 Application Circuits**

#### 4.9.1 BATTERY CURRENT SENSING

The MCP6141/2/3/4 op amps' Common Mode Input Range, which goes 0.3V beyond both supply rails, supports their use in high side and low side battery current sensing applications. The very low quiescent current (0.6 μA, typ.) help prolong battery life, and the rail-to-rail output supports detection low currents.

[Figure 4-9](#page-14-0) shows a high side battery current sensor circuit. The 1 k $\Omega$  resistor is sized to minimize power losses. The battery current (I<sub>DD</sub>) through the 1 kΩ resistor causes its top terminal to be more negative than the bottom terminal. This keeps the Common mode input voltage of the op amp at  $V_{DD}$ , which is within its allowed range. When no current is flowing, the output will be at its Maximum Output Voltage Swing  $(V<sub>OH</sub>)$ , which is virtually at  $V<sub>DD</sub>$ .



<span id="page-14-0"></span>*FIGURE 4-9: High Side Battery Current Sensor.*

#### 4.9.2 INVERTING SUMMING AMPLIFIER

The MCP6141/2/3/4 op amp is well suited for the inverting summing amplifier shown in [Figure 4-10](#page-14-1) when the resistors at the input  $(R_1, R_2,$  and  $R_3)$  make the noise gain at least 10 V/V. The output voltage  $(V<sub>OUT</sub>)$  is a weighted sum of the inputs  $(V<sub>1</sub>, V<sub>2</sub>,$  and  $V<sub>3</sub>)$ , and is shifted by the  $V_{RFF}$  input. The necessary calculations follow in [Equation 4-3](#page-14-2).



<span id="page-14-1"></span>

<span id="page-14-2"></span>**EQUATION 4-3:**

**Noise Gain:**  

$$
G_N = I + R_F \left( \frac{I}{R_I} + \frac{I}{R_2} + \frac{I}{R_3} \right) \ge 10 \text{ V/V}
$$

**Signal Gains:**

$$
G_1 = -R_F/R_1
$$
  
\n
$$
G_2 = -R_F/R_2
$$
  
\n
$$
G_3 = -R_F/R_3
$$

**Output Signal:**

$$
V_{OUT} = V_1 G_1 + V_2 G_2 + V_3 G_3 + V_{REF} G_N
$$

#### <span id="page-15-0"></span>**5.0 DESIGN TOOLS**

Microchip provides the basic design tools needed for the MCP6141/2/3/4 family of op amps.

#### **5.1 SPICE Macro Model**

The latest SPICE macro model for the MCP6141/2/3/4 op amps is available on our web site at www.microchip.com. This model is intended to be an initial design tool that works well in the op amp's linear region of operation at room temperature. See the model file for information on its capabilities.

Bench testing is a very important part of any design and cannot be replaced with simulations. Also, simulation results using this macro model need to be validated by comparing them to the data sheet specifications and characteristic curves.

#### **5.2 FilterLab® Software**

The FilterLab software is an innovative tool that simplifies analog active filter (using op amps) design. It is available free of charge from our web site at www.microchip.com. The FilterLab software tool provides full schematic diagrams of the filter circuit with component values. It also outputs the filter circuit in SPICE format, which can be used with the macro model to simulate actual filter performance.

#### <span id="page-16-0"></span>**6.0 PACKAGING INFORMATION**

#### **6.1 Package Marking Information**







6-Lead SOT-23 (**MCP6143)** Example:









#### 8-Lead MSOP **Example:**





#### **Package Marking Information (Continued)**

8-Lead PDIP (300 mil) Example: XXXXXXXX XXXXXNNN **K**YYWW ▔▂ ▂ ▁ ▁ ▏

8-Lead SOIC (150 mil) Example:



<u>nnr</u> **MCP6141 MCP61** I/P256 **OR** E/P<sup>(e3)</sup> 256 10536 **1** 0223 ਧਰਾਰਾ n n n **MCP6142** I/SN0223  $\circ$   $\Omega$  256



14-Lead PDIP (300 mil) (**MCP6144**) Example:





**OR** 



#### **Package Marking Information (Continued)**









#### **5-Lead Plastic Small Outline Transistor (OT) (SOT-23)**











**\*** Controlling Parameter

**Notes:**

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .005" (0.127mm) per side. EIAJ Equivalent: SC-74A

Drawing No. C04-091

Revised 09-12-05

#### **6-Lead Plastic Small Outline Transistor (CH) (SOT-23)**











**\*** Controlling Parameter

#### **Notes:**

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .005" (0.127mm) per side. BSC: Basic Dimension. Theoretically exact value shown without tolerances.

JEITA (formerly EIAJ) equivalent: SC-74A Drawing No. C04-120 See ASME Y14.5M

Revised 09-12-05

#### **8-Lead Plastic Micro Small Outline Package (MS) (MSOP)**











**\*** Controlling Parameter

**Notes:**

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .010" (0.254mm) per side.

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

See ASME Y14.5M

REF: Reference Dimension, usually without tolerance, for information purposes only.

See ASME Y14.5M

JEDEC Equivalent: MO-187

Drawing No. C04-111

Revised 07-21-05

#### **8-Lead Plastic Dual In-line (P) – 300 mil Body (PDIP)**









**\*** Controlling Parameter

**§** Significant Characteristic

**Notes:**

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .010" (0.254mm) per side. JEDEC Equivalent: MS-001

**8-Lead Plastic Micro Small Outline Package (MS) (MSOP)**









**\*** Controlling Parameter

**§** Significant Characteristic

**Notes:**

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .010" (0.254mm) per side. JEDEC Equivalent: MS-001

#### **14-Lead Plastic Dual In-line (P) – 300 mil Body (PDIP)**





**\*** Controlling Parameter

**§** Significant Characteristic

**Notes:**

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .010" (0.254mm) per side. JEDEC Equivalent: MS-001

**14-Lead Plastic Small Outline (SL) – Narrow, 150 mil Body (SOIC)**





**\*** Controlling Parameter

**§** Significant Characteristic

**Notes:**

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .010" (0.254mm) per side. JEDEC Equivalent: MS-012

#### **14-Lead Plastic Thin Shrink Small Outline (ST) – 4.4 mm Body (TSSOP)**











**\*** Controlling Parameter

**Notes:**

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .005" (0.127mm) per side. BSC: Basic Dimension. Theoretically exact value shown without tolerances.

See ASME Y14.5M

REF: Reference Dimension, usually without tolerance, for information purposes only.

See ASME Y14.5M

JEDEC Equivalent: MO-153 AB-1 Drawing No. C04-087

Revised: 08-17-05

**NOTES:**

#### <span id="page-28-0"></span>**APPENDIX A: REVISION HISTORY**

#### **Revision B (November 2005)**

The following is the list of modifications:

- 1. Added the following:
	- a) SOT-23-5 package for the MCP6141 single op amps.
	- b) SOT-23-6 package for the MCP6143 single op amps with Chip Select.
	- c) Extended Temperature (-40°C to +125°C) op amps.
- 2. Updated specifications in **[Section 1.0 "Electri](#page-1-0)[cal Characteristics"](#page-1-0)** for E-temp parts.
- 3. Corrected and updated plots in **[Section 2.0](#page-4-0) ["Typical Performance Curves"](#page-4-0)**.
- 4. Added **[Section 3.0 "Pin Descriptions"](#page-10-1)**.
- 5. Updated **[Section 4.0 "Applications Informa](#page-11-1)[tion"](#page-11-1)** and added section on unused op amps.
- 6. Updated **[Section 5.0 "Design Tools"](#page-15-0)** to include FilterLab.
- 7. Added SOT-23-5 and SOT-23-6 packages and corrected package marking information in **[Section 6.0 "Packaging Information"](#page-16-0)**.
- 8. Added **[Appendix A: "REVISION HISTORY"](#page-28-0)**.

#### **Revision A (September 2002)**

• Original Release of this Document.

**NOTES:**

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To order or obtain information, e.g., on pricing or delivery, refer to the factory or the listed sales office.



**NOTES:**

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