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FAN21SV06 — TinyBuck™ 6 A, 24V Single-Input Integrated Synchronous Buck Regulator with Synchronization Capability

Features

- Single-Supply Operation with 6 A Output Current
- Over 94% Efficiency
- Fully Synchronous Operation with Integrated Schottky Diode on Low-Side MOSFET Boosts **Efficiency**
- Single Supply Device for V_{IN} > 6.5 V 24 V
- Programmable Frequency Operation (200-600 KHz)
- **Externally Synchronizable Clock with Master/Slave Provisions**
- Wide Input Range with Dual Supply: 3.0 V to 24 V
- Output Voltage Range: 0.8 V to $80\%V_{\text{IN}}$
- Power-Good Signal
- Accepts Ceramic Capacitors on Output
- External Compensation for Flexible Design
- Starts Up on Pre-Bias Outputs
- Integrated Bootstrap Diode
- Programmable Over-Current Protection
- Under-Voltage, Over-Voltage, and Thermal-Shutdown Protections
- 5 x 6 mm, 25-pin, 3-pad MLP

Applications

- Servers & Telecom
- Graphics Cards & Displays
- High-End Computing Systems
- Set-Top Boxes & Game Consoles
- Point-of-Load Regulation

Description

The FAN210SV06 TinyBuckTM is a highly efficient, small-footprint, programmable-frequency, 6 A integrated synchronous buck regulator.

FAN21SV06 contains both synchronous MOSFETs and a controller/driver with optimized interconnects in one package, which enables designers to solve high-current requirements in a small area with minimal external components, thereby saving cost. On-board internal 5 V regulator enables single-supply operation for input voltages >6.5 V.

The FAN21SV06 can be configured to drive multiple slave devices OR synchronize to an external system clock. In slave mode, FAN21SV06 may be set up to be free-running in the absence of a master clock signal.

External compensation, programmable switching frequency, and current-limit features allow for design optimization and flexibility. High-frequency operation allows for all ceramic solutions.

Fairchild's advanced BiCMOS power process combined with low- $R_{DS(ON)}$ internal MOSFETs and a thermally efficient MLP package provide the ability to dissipate high power in a small package. Integration helps to minimize critical inductances making layout simpler and more efficient compared to discrete solutions.

Output over-voltage, under-voltage, over-current and thermal-shutdown protections help protect the device from damage during fault conditions. FAN21SV06 prevents pre-biased output discharge during startup in point-of-load applications.

Related Resources

- *[TinyCalc™ Calculator Design Tool](http://www.fairchildsemi.com/an/AN/AN-6033.pdf) AN-6033 — FAN21SV06 Design Guide*
- *[AN-8022 TinyCalc™ Calculator](http://www.fairchildsemi.com/an/AN/AN-8022.pdf)*

Ordering Information

Pin Configuration

Figure 3. MLP 5 x 6 mm Pin Configuration (Bottom View)

Pad / Pin Definitions

Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Recommended Operating Conditions

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

Thermal Information

Note:

1. Typical thermal resistance when mounted on a four-layer, two-ounce PCB, as shown in Figure 37. Actual results are dependent upon mounting method and surface related to the design.

Electrical Characteristics

Note:

2. Specifications guaranteed by design and characterization; not production tested.

Electrical Characteristics (Continued)

Recommended operating conditions using the circuit in Figure 1 with V_{IN} , VIN_Reg=12 V, unless otherwise noted.

Note:

3. Delay times are not tested in production. Guaranteed by design.

Typical operating characteristics using the circuit shown in Figure 10, unless otherwise specified.

Circuit Operation

PWM Generation

Refer to Figure 2 for the PWM control mechanism. FAN21SV06 uses the summing-mode method of control to generate the PWM pulses. An amplified currentsense signal is summed with an internally generated ramp and the combined signal is compared with the output of the error amplifier to generate the pulse width to drive the high-side MOSFET. Sensed current from the previous cycle is used to modulate the output of the summing block. The output of the summing block is also compared against a voltage threshold set by the R_{LIM} resistor to limit the inductor current on a cycle-by-cycle basis. The controller facilitates external compensation for enhanced flexibility.

Initialization

Once VIN_Reg voltage exceeds the UVLO threshold and EN is high, the IC checks for an open or shorted FB pin before releasing the internal soft-start ramp (SS).

If R1 is open (Figure 1), error amplifier output (COMP) is forced LOW and no pulses are generated. After the SS ramp times out (T1.0), an under-voltage fault occurs.

If the parallel combination of R1 and R_{BIAS} is \leq 1 kΩ, the internal SS ramp is not released and the regulator does not start.

Internal Regulator

FAN21SV06 facilitates single-supply operation for input voltages >6.5 V. At startup, the output of the internal regulator tracks the input voltage and comes into regulation (5 V) when VIN_Reg exceeds the UVLO threshold. The EN pin is released at the same time. The output voltage of the internal regulator $(5 V$ Reg) is set to 5 V. The internal regulator supplies power to all the control circuits including the drivers.

For applications with V_{IN} <6.5 V, FAN21SV06 can be used if VIN_Reg is provided with a separate low-power source >6.5 V. VIN_Reg supply should come up after VIN during dual-supply operation. The VIN_Reg pin should always be decoupled with at least $1 \mu F$ ceramic capacitor (see Figure 11).

Since V_{CC} is used to drive the internal MOSFET gates, high peak currents are present on the 5V_Reg pin. Connect a >2.2 µf X5R or X7R decoupling capacitor between the 5 V_Reg pin and PGND.

In addition to supplying power for the control circuits internally, 5 V_Reg output can be used as a reference voltage for other applications requiring low noise reference voltage. 5 V_Reg is capable of sourcing up to 5 mA of output current.

When EN is pulled LOW externally, 5 V_Reg output is still present but the IC is in standby mode with no switching.

Soft-Start

FAN21SV06 uses an internal digital soft-start circuit to slowly ramp up the output voltage and limit inrush current during startup. When $5 \vee$ Reg is in regulation and EN is high, the circuit releases SS and enables the PWM regulator. Soft-start time is a function of switching frequency (number of clock cycles).

Once internal SS ramp has charged to 0.8 V (T0.8), the output voltage is in regulation. Until SS ramp reaches 1.0 V (T1.0), only over-current-protection circuit is active during soft-start and all other output protections are inhibited.

In dual-supply operation mode, it is necessary to apply VIN before VIN_Reg reaches its UVLO threshold to avoid skipping the soft-start cycle.

Figure 30. Typical Soft-Start Timing Diagram

VIN Reg UVLO or toggling the EN pin discharges the SS and resets the IC.

Startup on Pre-Bias

The regulator does not allow the low-side MOSFET to operate in full synchronous mode until SS reaches 95% of V_{REF} (~0.76 V). This enables the regulator to startup on a pre-biased output and ensures that output is not discharged during the soft-start cycle.

Protections

The converter output is monitored and protected against extreme overload, short-circuit, over-voltage, and undervoltage conditions.

Under-Voltage Protection

If FB remains below the under-voltage threshold for 16 consecutive clock cycles, the fault latch is set and the converter shuts down. This fault is prevented from setting the fault latch during soft-start.

Over-Voltage Protection

If FB exceeds 115% \bullet V_{REF} for two consecutive clock cycles, the fault latch is set and shutdown occurs.

A shorted high-side MOSFET condition is detected when SW voltage exceeds ~0.7 V while the low-side MOSFET is fully enhanced. The fault latch is set immediately upon detection.

These two fault conditions are allowed to set the fault latch at any time, including during soft-start.

Over-Temperature Protection

The chip incorporates an over-temperature-protection circuit that sets the fault latch when a die temperature of about 155°C is reached. The IC is allowed to restart when the die temperature falls below 125°C.

EN / Auto-Restart

After a fault, EN pin is discharged with 1 µA current pull down to a 1.1 V threshold before the internal 800 kΩ pull up is restored. A new soft-start cycle begins when EN charges above 1.35 V.

Depending on the external circuit, the FAN21SV06 can be configured to remain latched off or automatically restart after a fault, as listed in Table 1.

Table 1. Fault / Restart Configurations

With EN left open, restart is immediate.

If auto-restart is not desired, tie the EN pin high with a logic gate to keep the 1 µA current sink from discharging EN to 1.1 V. Figure 31 shows one method to pull up EN to V_{CC} for a latch configuration.

Figure 31. Enable Control with Latch Option

Power Good (PGOOD) Signal

PGOOD is an open-drain output that asserts LOW when V_{OUT} is out of regulation, as measured at the FB pin. The thresholds are specified in the Electrical Specifications section. PGOOD does not assert HIGH until soft start is complete (T1.0).

Application Information

Setting the Output Voltage

The output voltage of the regulator can be set from 0.8 V to ~80% of V_{IN} by an external resistor divider (R1 and R_{BIAS} in Figure 1). For output voltages >3.3 V, output current rating may need to be de-rated depending on the ambient temperature, power dissipated in the package and the PCB layout. (Refer to Thermal Information table and Figure 29.)

The internal reference is set to 0.8 V with 650 nA sourced from the FB pin to ensure that the regulator does not start if the pin is left open.

The external resistor divider is calculated using:

$$
\frac{0.8V}{R_{BIAS}} = \frac{V_{OUT} - 0.8V}{R1} + 650nA
$$
 (1)

Connect R_{BIAS} between FB and AGND.

Setting the Clock Frequency

Oscillator frequency is determined by a resistor, R_T that is connected between the (R_T) pin and AGND (Master Mode) or 5 V Reg (Slave Mode):

$$
f_{(KHz)} = \frac{10^6}{(65 \cdot R_T) + 135}
$$
 (2)

where R_T is expressed in kΩ.

$$
R_{T(K\Omega)} = \frac{(10^6/f) - 135}{65} \tag{3}
$$

where frequency (f) is expressed in KHz. In slave mode, the switching frequency is about 10% slower for the same R_T .

The regulator does not start if R_T is open in Master mode.

Calculating the Inductor Value

Typically the inductor value is chosen based on ripple current (ΔI) which is chosen between 10 to 35% of the maximum DC load. Regulator designs that require fast transient response use a higher ripple-current setting while regulator designs that require higher efficiency keep ripple current on the low side and operate at a lower switching frequency.

$$
\Delta I L = \frac{V_{\text{OUT}} \bullet (1-D)}{L \bullet f} \tag{4}
$$

where f is the oscillator frequency, and

$$
L = \frac{V_{\text{OUT}} \bullet (1 - D)}{\Delta l \cdot \bullet f} \tag{5}
$$

Setting the Ramp-Resistor Value

As a starting point, set the internal ramp amplitude (ΔV_{RAMP}) to 0.5 V. R_{RAMP} is approximately:

$$
R_{RAMP(K\Omega)} = \frac{(V_{IN} - 1.8) \bullet V_{OUT}}{18 \times 10^{-6} \bullet V_{IN} \bullet f} - 2
$$
 (6)

where frequency (f) is expressed in KHz.

Refer to [AN-6033 — FAN21SV06 Design Guide](http://www.fairchildsemi.com/an/AN/AN-6033.pdf) to determine the optimal R_{RAMP} value.

Setting the Current Limit

The current limit system involves two comparators. The MAX I_{LIMIT} comparator is used with a V_{LIM} fixed-voltage reference and represents the maximum current limit allowable. This reference voltage is temperature compensated to reflect the R_{DSON} variation of the lowside MOSFET. The ADJUST I_{LIMIT} comparator is used where the current limit needs to be set lower than the V_{IUM} fixed reference. The 10 μ A current source does not track the R_{DSON} changes over temperature, so change is added into the equations for calculating the ADJUST I_{LIMIT} comparator reference voltage, as is shown below. Figure 32 shows a simplified schematic of the overcurrent system.

Figure 32. Current-Limit System Schematic + \overline{a} $\mathsf{V_{cc}}$ 10µA ILIMIT ILIM RILIM + \overline{a} ILIMIT ADJUST MAX + _ COMP PWM VERR PWM ILIMTRIP VILIM RAMP

Since the I_{LIM} voltage is set by a 10 μ A current source into the R_{ILM} resistor, the basic equation for setting the reference voltage is:

 $V_{\text{RII IM}} = 10 \mu A^* R_{\text{II IM}}$ (7)

To calculate $R_{\text{II-M}}$:

$$
R_{\text{ILIM}} = V_{\text{RILIM}} / 10 \mu A \tag{8}
$$

The voltage V_{RILIM} is made up of two components, V_{BOT} (which relates to the current through the low-side MOSFET) and V_{RMPEAK} (which relates to the peak current through the inductor). Combining those two voltage terms results in:

$$
R_{ILIM} = (V_{BOT} + V_{RMPEAK}) / 10 \mu A \tag{9}
$$

 $R_{ILIM} = \{0.96 + (I_{LOAD} * R_{DSON} * K_T * 8)\}$ + R_{lLIM} = {0.96 + (I_{LOAD} * R_{DSON} *K_T*8)} + (10)
{D*(V_{IN} – 1.8)/(f_{SW}*0.03*10^-3*R_{RAMP})}/10µA

where:

 $V_{\text{ROT}} = 0.96 + (I_{\text{LOAD}} * R_{\text{DSON}} * K_{\text{T}} * 8);$

 $V_{RMPEAK} = D^*(V_{IN} - 1.8)/(f_{SW}^* 0.03^* 10^{(-0.3*} R_{RAMP});$

 I_{LOAD} = the desired maximum load current;

 R_{DSON} = the nominal R_{DSON} of the low-side MOSFET;

 K_T = the normalized temperature coefficient for the low-side MOSFET (on datasheet graph);

 $D = V_{\text{OUT}}/V_{\text{IN}}$ duty cycle;

 f_{SW} = Clock frequency in kHz; and

 R_{RAMP} = chosen ramp resistor value in kΩ.

After 16 consecutive, pulse-by-pulse, current-limit cycles, the fault latch is set and the regulator shuts down. Cycling V_{CC} or EN restores operation after a normal soft-start cycle *(refer to the Auto-Restart section)*.

The over-current protection fault latch is active during the soft-start cycle. Use 1% resistor for R_{HIM} .

Loop Compensation

The control loop is compensated using a feedback network around the error amplifier. Figure 33 shows a complete Type-3 compensation network. Type-2 compensation eliminates R3 and C3.

Figure 33. Compensation Network

Since the FAN21SV06 employs summing current-mode architecture, Type-2 compensation can be used for many applications. For applications that require wide loop bandwidth and/or use very low-ESR output capacitors, Type-3 compensation may be required.

R_{RAMP} provides feedforward compensation for changes in V_{IN} . With a fixed R_{RAMP} value, the modulator gain increases as V_{IN} is reduced, which could make it difficult to compensate the loop. For low-input-voltage-range designs (3 V to 8 V), R_{RAMP} and the compensation component values are going to be different as compared to designs with V_{IN} between 8 V and 24 V.

Master/Slave Configuration

When first enabled, the IC determines if it is configured as a master or slave for synchronization, depending on how R_T is connected.

Table 2. Master / Slave Configuration

R_T to:	Master / Slave	CLK Pin
GND	Master	Output
5V Reg	Slave, free-running	Input

Slaves free-run in the absence of an external clock signal input when R_T is connected to 5 V_Reg, allowing regulation to be maintained. It is not recommended to leave R_T open when running in slave mode to avoid noise pick up on the clock pin.

Slave free-running frequency should be set at least 25% lower than the incoming synchronizing pulse frequency. Maximum synchronizing clock frequency is recommended to be below 600 KHz.

Synchronization

The synchronization method employed by the FAN21SV06 also provides the following features for maximum flexibility.

- Synchronization to an external system clock
- Multiple FAN21SV06s can be synchronized to a single master or system clock
- Independently programmable phase adjustment for one or multiple slaves
- Free-running capability in the absence of system clock or, if the master is disabled/faulted, the slaves can continue to regulate at a lower frequency

The FAN21SV06 master outputs an 85 ns-wide clock (CLK) signal, delayed 180 $^{\circ}$ from its leading PWM edge. This feature allows out-of-phase operation for the slaves, thereby reducing the input capacitance requirements when more than one converter is operating on the same input supply. The leading SW-node edge is delayed ~40 ns from the rising PWM signal.

On a slave, synchronization is rising-edge triggered. The CLK input pin has a 1.8 V threshold and a 200 µA current source pull-up.

In Master mode, the clock signals go out after power-good signal asserts high. Likewise, in Slave mode synchronization to an external clock signal occurs after the power-good signal goes high. Until then, the converter operates in free-run mode.

Figure 34. Synchronization Timing Diagram

Figure 35. Slave-CLK-Input Block Diagram

One or more slaves can be connected directly to a master or system clock to achieve a 180 $^{\circ}$ phase shift.

Figure 36. Slaves with 180° Phase Shift

Since the synchronizing circuit utilizes a narrow reset pulse, the actual phase delay is slightly more than 180° .

The FAN21SV06 is not intended for use in single-output, multi-phase regulator applications.

PCB Layout

Good PCB layout and careful attention to temperature rise is essential for reliable operation of the regulator. Four-layer PCB with 2-ounce copper on the top and bottom side and thermal vias connecting the layers is recommended. Keep power traces wide and short to minimize losses and ringing. Do not connect AGND to PGND below the IC. Connect AGND pin to PGND at the output OR to the PGND plane.

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