

# **MCP1612**

# **Single 1A 1.4 MHz Synchronous Buck Regulator**

#### **Features**

- Fixed Switching Frequency: 1.4 MHz
- Input Operating Voltage Range: 2.7V to 5.5V
- Integrated Buck and Synchronous Switches
- Adjustable Output Voltage Range: 0.8V to 5.0V
- 100% Duty Cycle Capable for Low Input Voltage
- Continuous Output Current Capability: 1A
- Shutdown Control with  $I<sub>O</sub> < 0.01 \mu A$  (Typical)
- Integrated Soft Start
- Integrated Undervoltage Lockout (UVLO) Protection
- Integrated Overtemperature Protection
- Fast Dynamic Response to Line and Load Steps
- Small, 8-Pin DFN and MSOP Packages
- Operating Temperature Range: -40°C to +85°C

#### **Applications**

- Network Interface Cards
- Portable Computers
- Set Top Boxes
- DSL Modems and Routers
- USB-Powered Devices
- GBIC Modules
- High-Speed Data System BUS Termination
- Medical Instruments
- Cellular/GSM/PHS Phones
- +5V or +3.3V Distributed Voltages

#### **Description**

The MCP1612 is a 1A, 1.4 MHz fully integrated current mode-controlled synchronous Buck regulator. The MCP1612 is packed in the 8-pin MSOP and the spacesaving 3 x 3 DFN package. The DFN package also provides a lower thermal resistance package option for high-power, high ambient temperature applications. With an input operating range of 2.7V to 5.5V, the MCP1612 is ideal for applications that are powered by one single-cell Li-Ion, 2 to 3 cell NiMH, NiCd or alkaline sources.

The output voltage of the MCP1612 is easily set over the range of 0.8V to 5.0V by using an external resistor divider. The external inductor and output capacitor size are minimized since an internally-fixed 1.4 MHz clock is used to set the switching frequency. The fixed clock allows for continuous, fixed-frequency PWM operation over the full load range.

The MCP1612 is designed to provide fast dynamic response to sudden changes in input voltage and load current to minimize the necessary amount of external output capacitance.

The MCP1612 can be used with ceramic, tantalum or aluminum electrolytic output capacitors. Ceramic capacitors with values as low as 4.7 µF can be used to keep the output ripple voltage low. For applications that require better load step performance, the value of the output capacitor can be increased to 47 µF.

Additional features integrated into the MCP1612 include shutdown capability, soft start, Undervoltage Lockout, overcurrent and overtemperature protection.

#### **Package Types**



#### **Functional Block Diagram**



# **Typical Application Circuit**



# **1.0 ELECTRICAL CHARACTERISTICS**

#### **Absolute Maximum Ratings †**



**† Notice:** Stresses above those listed under "Maximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at those or any other conditions above those indicated in the operational listings of this specification is not implied. Exposure to maximum rating conditions for extended periods may affect device reliability.

# **DC CHARACTERISTICS**

**Electrical Specifications:** Unless otherwise noted,  $V_{\text{IN}} = V_{\text{cc}} = V_{\text{SHDN}} = 3.3$ V,  $V_{\text{OUT}} = 1.8$ V,  $C_{\text{IN}} = C_{\text{OUT}} = 10$  µF, L = 3.3 µH,  $I_{\text{LOAD}}$  = 100 mA,  $T_A$  = +25°C. **Boldface** specifications apply over the  $T_A$  range of -40°C to +85°C.



<span id="page-3-0"></span>**Note** 1: The integrated MOSFET switches have an integral diode from the L<sub>X</sub> pin to V<sub>IN</sub> and from L<sub>X</sub> to P<sub>GND</sub>. In cases where these diodes are forward-biased, the package power dissipation limits must be adhered to. Thermal protection is not able to limit the junction temperature for these cases.

<span id="page-3-1"></span>**2:** UVLO is specified for a falling V<sub>IN</sub>. Once the UVLO is activated, the UVLO-<sub>HYS</sub> must be overcome before the device will return to operation.

# **DC CHARACTERISTICS (CONTINUED)**



**Note 1:** The integrated MOSFET switches have an integral diode from the L<sub>X</sub> pin to V<sub>IN</sub> and from L<sub>X</sub> to P<sub>GND</sub>. In cases where these diodes are forward-biased, the package power dissipation limits must be adhered to. Thermal protection is not able to limit the junction temperature for these cases.

2: UVLO is specified for a falling V<sub>IN</sub>. Once the UVLO is activated, the UVLO-<sub>HYS</sub> must be overcome before the device will return to operation.

# **TEMPERATURE SPECIFICATIONS**



# **2.0 TYPICAL PERFORMANCE CURVES**

**Note:** The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only. The performance characteristics listed herein are not tested or guaranteed. In some graphs or tables, the data presented may be outside the specified operating range (e.g., outside specified power supply range) and therefore outside the warranted range.

**Note:** Unless otherwise indicated,  $V_{IN} = V_{CC} = V_{\overline{SHDN}} = 3.3V$ ,  $C_{OUT} = C_{IN} = 10 \mu F$ , L = 3.3  $\mu$ H, I<sub>LOAD</sub> = 100 mA, T<sub>A</sub> = +25°C. **Boldface** specifications apply over the  $T_A$  range of -40°C to +85°C.



FIGURE 2-1: Efficiency vs. Load Current,  $V_{IN} = 3.3V$ .



FIGURE 2-2: Efficiency vs. Load Current,  $V_{IN} = 5.0 V.$ 



FIGURE 2-3: Output Voltage vs. Load Current.





**FIGURE 2-4:** Dropout Voltage vs. Load Current.



**FIGURE 2-5:** Input Quiescent Current vs. Input Voltage.



Input Voltage.

**FIGURE 2-6:** Oscillator Frequency vs.

# **TYPICAL PERFORMANCE CURVES (Continued)**

**Note:** Unless otherwise indicated, V<sub>IN</sub> = V<sub>CC</sub> = V<sub>SHDN</sub> = 3.3V, C<sub>OUT</sub> = C<sub>IN</sub> = 10 µF, L = 3.3 µH, I<sub>LOAD</sub> = 100 mA,  $T_\mathsf{A}$  = +25°C. **Boldface** specifications apply over the  $T_\mathsf{A}$  range of -40°C to +85°C.











**FIGURE 2-9:** Load Transient Response.



**FIGURE 2-10:** Load Transient Response.



**FIGURE 2-11:** Line Transient Response.



**FIGURE 2-12:** Line Transient Response.

# **TYPICAL PERFORMANCE CURVES (Continued)**

**Note:** Unless otherwise indicated, V<sub>IN</sub> = V<sub>CC</sub> = V<sub>SHDN</sub> = 3.3V, C<sub>OUT</sub> = C<sub>IN</sub> = 10 µF, L = 3.3 µH, I<sub>LOAD</sub> = 100 mA,  $T_\mathsf{A}$  = +25°C. **Boldface** specifications apply over the  $T_\mathsf{A}$  range of -40°C to +85°C.



**FIGURE 2-13:** Low Load Current Switching Waveform.



FIGURE 2-14: High Load Current Switching Waveform.

# **3.0 MCP1612 PIN DESCRIPTIONS**

The descriptions of the pins are listed in [Table 3-1.](#page-8-0)

Pin No.	<b>Name</b>	<b>Function</b>
	$V_{IN}$	Input Voltage Pin
2	$V_{\rm CC}$	Analog Input Voltage Pin
3	<b>SHDN</b>	Shutdown Control Input Pin
4	<b>COMP</b>	Transconductance Amplifier Output Pin
5	FB.	Feedback Input Pin
6	A <sub>GND</sub>	Analog Ground Pin
	$P_{GND}$	Power Ground Pin
8	L <sub>X</sub>	<b>Buck Inductor Output Pin</b>

<span id="page-8-0"></span>**TABLE 3-1: PIN FUNCTION TABLE**

# **3.1** Input Voltage Pin (V<sub>IN</sub>)

Connect the input voltage source to the  $V_{IN}$  pin. For normal operation, the voltage on the  $V_{IN}$  pin should be between +2.7V and +5.5V. A 10 µF bypass capacitor should be connected between the  $V_{IN}$  pin and the  $P_{GND}$ pin.

# **3.2** Analog Input Voltage Pin (V<sub>CC</sub>)

The  $V_{CC}$  pin provides bias for internal analog functions. This voltage is derived by filtering the  $V_{1N}$  supply.

# **3.3 Shutdown Input Pin (SHDN)**

Connect SHDN to a logic level input to turn the regulator on or off. A logic-high (>45% of  $V_{IN}$ ) will enable the regulator. A logic-low (<15% of  $V_{IN}$ ) will force the regulator into Shutdown mode. When in shutdown, both the P-Channel and N-Channel switches are turned off.

# **3.4 Compensation Pin (COMP)**

COMP is the internal transconductance amplifier output pin. External compensation is connected to the COMP pin for control-loop stabilization.

## **3.5 Feedback Pin (FB)**

Connect the output voltage of the Buck converter through an external resistor divider to the FB pin to regulate the output voltage. The nominal voltage that is compared to this input for pulse termination is 0.8V.

# **3.6** Analog Ground Pin (A<sub>GND</sub>)

Tie all small-signal ground returns to A<sub>GND</sub>. Noise on this ground can effect the sensitive internal analog measurements.

# **3.7 Power Ground Pin (P<sub>GND</sub>)**

Connect all large-signal ground returns to P<sub>GND</sub>. These large-signal traces should have a small loop area and length to prevent coupling of switching noise to sensitive traces.

# **3.8 Buck Inductor Output Pin (L<sub>X</sub>)**

Connect  $L_X$  directly to the Buck inductor. This pin carries large signal-level currents and all connections should be made as short as possible.

# **4.0 DETAILED DESCRIPTION**

#### **4.1 Device Overview**

The MCP1612 is a 1A Synchronous Buck converter switching at 1.4 MHz to minimize external component size and cost. While utilizing a fixed-frequency current mode architecture, the MCP1612 provides fast response to sudden load changes and overcurrent protection in the event of a shorted load. The input voltage range is 2.7V to 5.5V, while the output voltage is adjustable by properly setting an external resistor divider and can range from 0.8V to  $V_{IN}$ . Integrated soft start, Undervoltage Lockout (UVLO) and overtemperature protection minimize external circuitry and component count.

#### **4.2 Current Mode Control Scheme**

The MCP1612 incorporates a peak current mode control scheme. Peak Current mode is used to obtain high gain in the PWM control loop for very fast response to dynamic line and load conditions. With both the P-Channel and the N-Channel MOSFETs turned off, the beginning of a cycle occurs on the negative edge of the internal 1.4 MHz oscillator, the P-Channel MOSFET turns on and current ramps up into the Buck inductor. The inductor current is sensed and tied to one input of a high-speed comparator. The other input of the high-speed comparator is the error amplifier output. This is the amplified difference between the internal 0.8V reference and the divided down  $V_{\text{OUT}}$  signal at the Feedback pin of the MCP1612. When the sensed inductor current ramps up to the point that it is equal to the amplified error signal, the high-speed comparator output switches states and the P-Channel MOSFET is turned off until the beginning of the next clock cycle and the N-Channel is turned on. The width of the pulse or "duty cycle" is ideally determined by the  $V_{\text{OUT}}/V_{\text{IN}}$  ratio of the DC/DC converter. The actual duty cycle is slightly larger to account for the non-ideal losses of the integrated MOSFET switches and the losses in the external inductor.

#### **4.3 Low Dropout Operation**

The MCP1612 is capable of operating over a wide range of input voltages. The PWM architecture allows for the P-Channel MOSFET to achieve 100% duty cycle operation for applications that have minimal input voltage headroom. During 100% Duty Cycle mode, the output voltage  $(V_{\text{OUT}})$  = Output Current ( $I_{\text{OUT}}$ ) x Resistance (P-Channel  $R_{DSON} + R_{INDIICTOR}$ ).

#### **4.4 Current Limit**

Cycle-by-cycle current limit is used to protect the MCP1612 from being damaged when an external short circuit is applied. The typical peak current limit is 2.3A. If the sensed inductor current reaches the 2.3A limit, the P-Channel MOSFET is turned off, even if the output voltage is not in regulation.

#### **4.5 Soft Start**

During normal power-up as  $V_{IN}$  rises above the UVLO protection setting or, in the case of a logic-low to logichigh transition on the shutdown pin, the rise time of the MCP1612 output voltage is controlled by the soft start feature. This is accomplished by slowly allowing the output of the error amplifier to rise. This feature prevents the output voltage from overshooting the desired value and the sudden inrush of current, depleting the input capacitors and causing a large dip in input voltage. This large dip in the input voltage could trip the UVLO threshold, causing the converter to shutdown prior to reaching steady-state operation.

#### **4.6 Undervoltage Lockout (UVLO)**

The UVLO feature uses a comparator to sense the input voltage level  $(V_{IN})$ . If the input voltage is lower than the voltage necessary to properly operate the MCP1612, the UVLO feature will hold the converter off. When  $V_{IN}$  rises above the necessary input voltage, the UVLO is released and soft start begins. For the MCP1612, the UVLO protection threshold is a maximum of 2.7V. Hysteresis is built into the UVLO circuit to compensate for input impedance. For example, once the converter starts, if there is any resistance between the input voltage source and the converter, there will be a voltage drop at the converter input equal to  $I_{IN} \times R_{IN}$ . The typical hysteresis for the MCP1612 is 200 mV.

#### **4.7 Overtemperature Protection**

The MCP1612 has an integrated overtemperature protection circuit that monitors the device junction temperature and shuts the device off if the junction temperature exceeds the typical 160°C threshold. If the overtemperature threshold is reached, the soft start is reset so that when the junction temperature cools to approximately 151°C, the device will automatically restart and the output voltage will not overshoot.

#### **4.8 Shutdown Input Operation**

The SHDN pin is used to turn the MCP1612 on and off. When the SHDN pin is tied low, the MCP1612 is off. When tied high, the MCP1612 will be enabled and begin operation as long as the input voltage is not below the UVLO threshold.

# **5.0 APPLICATION CIRCUITS/INFORMATION**



**FIGURE 5-1:** Typical Application Circuit.

# **5.1 Typical Applications**

The MCP1612 Buck controller can be used in several different applications where a voltage that is lower than the supply voltage is required. The small size, low-cost, and high efficiency make the MCP1612 a good choice for densely packaged applications. The input voltage range, low dropout voltage and low shutdown current make this part perfectly suited for battery-powered applications.

# **5.2 Design Example**

The step-by-step design of a Buck converter with the following parameters is designed to show how easy the MCP1612 is to use.

Input voltage = 3.3V Output voltage = 1.2V Output current  $=$  0A to 1A Switching frequency = 1.4 MHz  $V_{\text{OUT}}$  = 1.2V

#### 5.2.1 SETTING OUTPUT VOLTAGE

The output voltage of the MCP1612 is set by using an external resistor divider network. The voltage present at the feedback input pin (FB) is internally compared to a 0.8V reference voltage. A 200 kΩ resistor is recommended for  $R_2$ , the lower end of the voltage divider. Using higher value resistors will make the circuit more susceptible to noise on the FB pin. Lower value resistors can be used, if necessary.

[Equation 5-1](#page-10-0) used to calculate the output voltage is shown below.

#### <span id="page-10-0"></span>**EQUATION 5-1:**

$$
R_I = R_2 \times \left(\frac{V_{OUT}}{V_{FB}} - I\right)
$$

Where:

 $V_{\text{OUT}}$  = desired output voltage

 $V_{FB}$  = MCP1612 internal reference voltage

- $R_1$  = top resistor value
- $R<sub>2</sub>$  = bottom resistor value

For this example:

 $V_{FB}$  = 0.8V  $R_2$  = 200 kΩ  $R_1$  = 100 kΩ

The MCP1612 is capable of a 15% duty cycle. Instability may result when the duty cycle is below 15%. If less than 15% duty cycle operation is needed, care must be taken to ensure stable operation.

#### 5.2.2 BUCK INDUCTOR

There are many requirements that need to be satisfied when selecting the Buck inductor. The application, physical size, current rating, resistance, mounting method, supplier, temperature range, minimum inductance and cost all need to be considered.

Many suppliers specify the maximum peak current that an inductor can handle before magnetic saturation occurs. The peak current is equal to the maximum DC output current, plus one-half the peak-to-peak AC ripple current.

When the P-Channel MOSFET is on, the current in the Buck inductor is ramped up. The voltage across the inductor, the inductance, and the MOSFET on time are required to determine the peak-to-peak ripple current.

When operating in continuous current mode, the ontime of the P-Channel MOSFET is determined by multiplying the duty cycle by the switching period. The following equation can be used to find the duty cycle.

#### **EQUATION 5-2:**

$$
DutyCycle = \frac{V_{OUT}}{V_{IN}}
$$

The on-time is then defined as follows.

#### **EQUATION 5-3:**

$$
T_{ON} = DutyCycle \times \frac{1}{F_{SW}}
$$

Where:

 $F_{SW}$  = switching frequency

The AC ripple current in the inductor can be calculated by the following relationship.

#### **EQUATION 5-4:**

$$
V_L = L \times \frac{\Delta I_L}{\Delta t}
$$

Solving for ∆I<sub>L</sub> yields:

#### **EQUATION 5-5:**

$$
\Delta I_L = \frac{V_L}{L} \times \Delta t
$$

Where:

$$
V_L
$$
 = voltage across the inductor ( $V_{IN} - V_{OUT}$ )  $\Delta t$  = on-time of the P-Channel MOSFET

The value of the Buck inductor is chosen to be 3.3 µH. The AC ripple current is controlled by the size of the Buck inductor. The value of the inductor will therefore need to be raised so that the converter operates in Continuous Conduction mode. Calculating the current rating of the Buck inductor follows:

$$
V_{IN} = 3.3V
$$
  
\n
$$
V_{OUT} = 1.2V
$$
  
\n
$$
F_{SW} = 1.4 MHz
$$
  
\n
$$
I_{OUT(MAX)} = 1A
$$
  
\n
$$
T_{ON} = (1.2V/3.3V) \times (1/1.4 MHz)
$$
  
\n
$$
T_{ON} = 260 ns
$$
  
\n
$$
V_{L} = (3.3V - 1.2V) = 2.1V
$$
  
\n
$$
\Delta I_{L} = (2.1V/3.3 \mu H) \times 260 ns
$$
  
\n
$$
\Delta I_{L} = 165 mA
$$
  
\n
$$
I_{L(PEAK)} = I_{OUT(MAX)} + 1/2 \Delta I_{L}
$$
  
\n
$$
I_{L(PEAK)} = 1A + (165 mA)/2
$$
  
\n
$$
I_{L(PEAK)} = 1.08A
$$

The inductor that is selected must have an inductance of 3.3 µH at a peak current rating of 1.08A. The DC resistance of the inductor should be as low as feasibly possible. Extremely low DC resistance inductors are available, but a trade-off between size and cost should be considered.

#### 5.2.3 OUTPUT CAPACITOR

The output capacitor is used to filter the inductor AC ripple current and provide storage for load transients. The size and Equivalent Series Resistance (ESR) of the output capacitor determines the amount of ripple voltage present at the output of the converter. When selecting the output capacitor, a design trade-off has to be made between the acceptable ripple voltage and the size/cost of the output capacitor. Ceramic capacitors have very low ESR, but increase in cost with higher values. Tantalum and Electrolytic capacitors are relatively inexpensive in higher values, but they also have a much higher ESR.

The amount of capacitance needed to obtain the desired ripple voltage is calculated by using the following relationship:

#### **EQUATION 5-6:**

$$
I_C = C \times \frac{\Delta V_C}{\Delta t}
$$

Solving for C:

$$
C = I_C \times \frac{\Delta t}{\Delta V_C}
$$

Where:

- $I_C$  = peak-to-peak ripple current
- ∆t = on-time of P-Channel MOSFET
- $\Delta V_C$  = output ripple voltage

There will also be some ripple voltage caused by the ESR of the capacitor. The ripple is defined as follows.

#### **EQUATION 5-7:**

 $V_{ESRRIPPIF} = ESR \times I_C$ 

For this example:



#### 5.2.4 INPUT CAPACITOR

For the Buck topology, the input current is pulled from the source and the input capacitor in pulses. The size of the input capacitor will determine the amount of current pulled from the source. For most applications, a 10 µF ceramic capacitor connected between the MCP1612  $V_{IN}$  and  $P_{GND}$  is recommended to filter the current pulses. Less capacitance can be used for applications that have low source impedance. The ripple current rating for ceramic capacitors are typically very high due to their low loss characteristics. Low-cost electrolytic capacitors can be used, but their ripple current rating should not be exceeded.

#### $5.2.5$  V<sub>CC</sub> INPUT

The  $V_{CC}$  input is used to bias the internal MCP1612 circuitry. A 10 $\Omega$  resistor is recommended between the unregulated input  $V_{IN}$  and  $V_{CC}$ , along with a 0.1  $\mu$ F capacitor to ground to help isolate the  $V_{CC}$  pin from the switching noise.

#### 5.2.6 COMPENSATION COMPONENTS

An internal transconductance error amplifier is used to compensate the Buck converter. An external resistor  $(R_C)$  and capacitor  $(C_C)$ , connected between COMP and GND, are all that is needed to provide a highbandwidth loop.

[Table 5-1](#page-12-0) identifies values for  $R<sub>C</sub>$  and  $C<sub>C</sub>$  for standard Buck inductor, L, and output capacitor,  $C_{\text{OUT}}$ , values.

<span id="page-12-0"></span>



#### **5.3 Printed Circuit Board Layout**

The MCP1612 is capable of switching over 1A at 1.4 MHz. As with all high-frequency switching power supplies, good board layout techniques are essential to prevent noise generated by the switching power-train from interfering with the sensing circuitry.

There are two ground pins ( $P_{GND}$  and  $A_{GND}$ ) on the MCP1612 to separate the large-signal ground current from the small-signal circuit ground. These two grounds should be kept separate and only connected together near the input bulk capacitor.

Care must also be taken to minimize the length and loop area of the large-signal connections. Components connected to this loop consist of the input bulk capacitor,  $V_{IN}$ ,  $P_{GND}$ , and  $L_X$  pins of the MCP1612, the Buck inductor and the output filter capacitor.

# **6.0 PACKAGING INFORMATION**

#### **6.1 Package Marking Information (Note)**



8-Lead DFN (3mm x 3mm) Example:







The DFN package for this device has not been qualified at the time of this publication. Contact your Microchip Sales Office for availability.

**NOTE:** These devices are being released in PB-free packaging.



**\*** Standard marking consists of Microchip part number, year code, week code, and traceability code.









\*Controlling Parameter

Notes:

Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed .010" (0.254mm) per side.

JEDEC Equivalent: MO-187

Drawing No. C04-111

## **8-Lead Plastic Dual Flat No Lead Package (MF) 3x3x0.9 mm Body (DFN) – Saw Singulated**

The DFN package for this device has not been qualified at the time of this publication. Contact your Microchip Sales Office for availability.





\*Controlling Parameter

Notes:

1. Package may have one or more exposed tie bars at ends.

2. Pin 1 visual index feature may vary, but must be located within the hatched area.

Exposed pad dimensions vary with paddle size. 3.

4. JEDEC equivalent: MO-229

Drawing No. C04-062

Revised 05/24/04

# **APPENDIX A: REVISION HISTORY**

## **Revision A (December 2004)**

• Original data sheet release.

**NOTES:**

# **PRODUCT IDENTIFICATION SYSTEM**

To order or obtain information, e.g., on pricing or delivery, refer to the factory or the listed sales office.



## **Sales and Support**

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