## STEP-UP, SUPER-SMALL PACKAGE, 1.2 MHz <br> PWM / PFM SWITCHABLE SWITCHING REGULATOR

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The S-8363 Series is a CMOS step-up switching regulator which consists of a reference voltage source, an oscillation circuit, an error amplifier, a phase compensation circuit, a current limit circuit, and a start-up circuit.
Due to the operation of the PWM / PFM switching control, pulses are skipped under the light load operation and the S-8363 Series prevents decrease in efficiency caused by IC's operating current.
The S-8363 Series is capable of start-up from 0.9 V (lout $=1 \mathrm{~mA}$ ) by the start-up circuit, and is suitable for applications which use one dry cell.
The output voltage is freely settable from 1.8 V to 5.0 V by external parts.
Ceramic capacitors can be used for output capacitor. Small packages SNT-6A and SOT-23-6 enable high-density mounting.

## ■ Features

- Low operation voltage
- Oscillation frequency
- Input voltage range
- Output current
- Reference voltage
- Efficiency
- Soft start function
- Low current consumption
- Duty ratio
- Power-off function
- Current limit circuit
- Nch power MOS FET ON resistance
- Start-up function
- Lead-free, Sn 100\%, halogen-free ${ }^{* 1}$
: Start-up from 0.9 V (lout $=1 \mathrm{~mA}$ ) guaranteed
: 1.2 MHz
: 0.9 V to 4.5 V
$: 300 \mathrm{~mA}\left(\mathrm{~V}_{\text {IN }}=1.8 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=3.3 \mathrm{~V}\right)$
: $0.6 \mathrm{~V} \pm 2.5 \%$
: 85\%
: 1.2 ms typ.
: During switching-off, $95 \mu \mathrm{~A}$ typ.
: PWM / PFM switching control max.88\%
: Current consumption during power-off $3.0 \mu \mathrm{~A}$ max.
: limits the peak value of inductor current
: $0.25 \Omega$ typ.
: Operation with fixed duty pulse under the $\mathrm{V}_{\text {out }}$ voltage of 1.4 V or less
*1. Refer to " $\square$ Product Name Structure" for details.


## Applications

- MP3 players, digital audio players
- Digital cameras, GPS, wireless transceiver
- Portable devices


## ■ Packages

- SNT-6A
- SOT-23-6


## ■ Block Diagram



Figure 1

## ■ Product Name Structure

Users can select the packages for the S-8363 Series. Refer to "1. Product name" regarding the contents of product name, "2. Package" regarding the package drawings and "3. Product list" regarding the product type.

1. Product name

S-8363B - $\frac{\mathbf{x x x x}}{L^{\mathbf{U}}}{ }^{\mathbf{U}}{ }^{\text {Environmental code }}$
U: Lead-free (Sn 100\%), halogen-free

Package name (abbreviation) and IC packing specification* ${ }^{* 1}$
I6T1: SNT-6A, Tape M6T1: SOT-23-6, Tape
*1. Refer to the tape specification.
2. Package

| Package name | Drawing code |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Package | Tape | Reel | Land |
| SNT-6A | PG006-A-P-SD | PG006-A-C-SD | PG006-A-R-SD | PG006-A-L-SD |
| SOT-23-6 | MP006-A-P-SD | MP006-A-C-SD | MP006-A-R-SD | - |

3. Product list

Table 1

| SNT-6A | SOT-23-6 |
| :---: | :---: |
| S-8363B-I6T1U2 | S-8363B-M6T1U2 |

Remark Please select products of environmental code $=\mathrm{U}$ for $\mathrm{Sn} 100 \%$, halogen-free products.

## ■ Pin Configurations

SNT-6A
Top view


Figure 2

Table 2 SNT-6A

| Pin No. | Symbol | Description |
| :---: | :---: | :--- |
| 1 | FB | Output voltage feedback pin |
| 2 | VSS | GND pin |
| 3 | CONT | External inductor connection pin |
| 4 | VIN | IC power supply pin |
| 5 | VOUT | Output voltage pin |
| 6 | ON/ $\overline{\text { FFF }}$ | Power-off pin <br> "H" : Power-on (normal operation) <br> "L" : Power-off (standby) |

Table 3 SOT-23-6
SOT-23-6
Top view


| Pin No. | Symbol | Description |
| :---: | :---: | :--- |
| 1 | ON/ $\overline{\text { OFF }}$ | Power-off pin <br> "H" : Power-on (normal operation) <br> "L" : Power-off (standby) |
| 2 | VOUT | Output voltage pin |
| 3 | VIN | IC power supply pin |
| 4 | CONT | External inductor connection pin |
| 5 | VSS | GND pin |
| 6 | FB | Output voltage feedback pin |

Figure 3

## Absolute Maximum Ratings

Table 4 Absolute Maximum Ratings

| Item |  | Symbol | Absolute Maximum Ratings | Unit |
| :---: | :---: | :---: | :---: | :---: |
| VIN pin voltage |  | V IN | $\mathrm{V}_{\text {SS }}-0.3$ to $\mathrm{V}_{\text {SS }}+5.0$ | V |
| VOUT pin voltage |  | $V_{\text {OUT }}$ | $\mathrm{V}_{\text {SS }}-0.3$ to $\mathrm{V}_{\text {SS }}+6.0$ | V |
| FB pin voltage |  | $\mathrm{V}_{\text {FB }}$ | $\mathrm{V}_{\text {SS }}-0.3$ to $\mathrm{V}_{\text {Out }}+0.3$ | V |
| CONT pin voltage |  | $V_{\text {CONT }}$ | $\mathrm{V}_{\mathrm{ss}}-0.3$ to $\mathrm{V}_{\mathrm{ss}}+6.0$ | V |
| ON/OFF pin voltage |  | Von/OFF | $\mathrm{V}_{\text {SS }}-0.3$ to $\mathrm{V}_{\text {IN }}+0.3$ | V |
| Power Dissipation | SNT-6A | PD | $400^{* 1}$ | mW |
|  | SOT-23-6 |  | $650{ }^{* 1}$ | mW |
| Operating ambient temperature |  | $\mathrm{T}_{\text {opr }}$ | -40 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature |  | $\mathrm{T}_{\text {stg }}$ | -40 to +125 | ${ }^{\circ} \mathrm{C}$ |

*1. When mounted on board
[Mounted board]
(1) Board size : $114.3 \mathrm{~mm} \times 76.2 \mathrm{~mm} \times \mathrm{t} 1.6 \mathrm{~mm}$
(2) Name : JEDEC STANDARD51-7

Caution The absolute maximum ratings are rated values exceeding which the product could suffer physical damage. These values must therefore not be exceeded under any conditions.


Figure 4 Package Power Dissipation (When Mounted on Board)

## ■ Electrical Characteristics

Table 5 Electrical Characteristics
( $\mathrm{V}_{\text {IN }}=1.8 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=3.3 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ unless otherwise specified)

| Item | Symbol | Conditions | Min. | Typ. | Max. | Unit | Test Circuit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operating start voltage ${ }^{* 1}$ | $\mathrm{V}_{\text {ST }}$ | $\mathrm{I}_{\text {OUT }}=1 \mathrm{~mA}, \mathrm{~V}_{\text {OUT(S) }}{ }^{*}{ }^{2}=3.3 \mathrm{~V}$ | - | - | 0.9 | V | 2 |
| Operating input voltage | $\mathrm{V}_{\text {IN }}$ | - | - | - | 4.5 | V | 2 |
| Output voltage range | Vout(R) | - | 1.8 | - | 5.0 | V | 2 |
| FB voltage | $V_{\text {FB }}$ | - | 0.585 | 0.600 | 0.615 | V | 1 |
| FB voltage temperature coefficient | $\begin{aligned} & \hline \Delta \mathrm{V}_{\mathrm{FB}} \\ & \Delta \mathrm{Ta} \\ & \hline \end{aligned}$ | $\mathrm{Ta}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | - | $\pm 100$ | - | ppm $/{ }^{\circ} \mathrm{C}$ | 1 |
| FB pin input current | $\mathrm{I}_{\text {FB }}$ | $\mathrm{V}_{\text {OUT }}=1.8 \mathrm{~V}$ to 5.5 V , FB pin | -0.1 | - | +0.1 | $\mu \mathrm{A}$ | 1 |
| Current consumption during operation | $\mathrm{I}_{1 \times 1}$ | During switching, at no load$V_{F B}=V_{F B(S)}{ }^{* 3} \times 0.95$ | - | 6 | 15 | $\mu \mathrm{A}$ | 1 |
|  | $\mathrm{I}_{\text {s1 }}$ |  | - | 450 | 650 | $\mu \mathrm{A}$ | 1 |
| Current consumption during switching off | $\mathrm{l}_{1 \times 2}$ | During switching stop $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB}(\mathrm{S})} \times 1.1$ | - | 6 | 15 | $\mu \mathrm{A}$ | 1 |
|  | $\mathrm{I}_{\text {SS2 }}$ |  | - | 95 | 150 | $\mu \mathrm{A}$ | 1 |
| Current consumption during power-off | Isss | $\begin{aligned} & \mathrm{V}_{\text {ON }} / \overline{\text { OFF }}=0 \mathrm{~V}, \\ & \mathrm{~V}_{\text {IN }}=\mathrm{V}_{\text {OUT }}=4.5 \mathrm{~V} \\ & \hline \end{aligned}$ | - | - | 3.0 | $\mu \mathrm{A}$ | 1 |
| Oscillation frequency | fosc | - | 1.0 | 1.2 | 1.4 | MHz | 2 |
| Maximum duty ratio | MaxDuty | $\mathrm{V}_{\mathrm{FB}}=\mathrm{V}_{\mathrm{FB}(\mathrm{S})} \times 0.95$ | 82 | 88 | 94 | \% | 2 |
| PWM / PFM switching duty ratio | PFMDuty | - | - | 13 | - | \% | 2 |
| Power MOS FET ON resistance ${ }^{* 4}$ | $\mathrm{R}_{\text {NFET }}$ | - | - | 0.25 | - | $\Omega$ | 1 |
| Power MOS FET leakage current | LLSW | Von/ $\overline{\text { OFF }}=0 \mathrm{~V}$ | - | 0.01 | 0.5 | $\mu \mathrm{A}$ | 1 |
| Limited current | LİM | - | 0.9 | 1.1 | 1.3 | A | 3 |
| High level input voltage | $\mathrm{V}_{\text {SH }}$ | $\mathrm{V}_{\text {IN }}=1.8 \mathrm{~V}$ to 4.5 V , ON/ $\overline{\mathrm{FFF}}$ pin | 0.75 | - | - | V | 1 |
| Low level input voltage | $\mathrm{V}_{\text {SL }}$ | $\mathrm{V}_{\mathrm{IN}}=1.8 \mathrm{~V}$ to 4.5 V , ON/OFF pin | - | - | 0.25 | V | 1 |
| High level input current | $\mathrm{I}_{\text {SH }}$ | $\mathrm{V}_{\mathrm{IN}}=1.8 \mathrm{~V}$ to 4.5 V , ON/ $\overline{\mathrm{FFF}}$ pin | -0.1 | - | 0.1 | $\mu \mathrm{A}$ | 1 |
| Low level input current | $\mathrm{I}_{\text {SL }}$ | $\mathrm{V}_{\mathrm{IN}}=1.8 \mathrm{~V}$ to 4.5 V , ON/OFF pin | -0.1 | - | 0.1 | $\mu \mathrm{A}$ | 1 |
| Soft-start time ${ }^{* 5}$ | $\mathrm{t}_{\text {ss }}$ | - | 0.6 | 1.2 | 1.8 | ms | 2 |

*1. This is the guaranteed value measured with external parts shown in "Table 6 External Parts List" and with test circuits shown in Figure 6. The operating start voltage varies largely depending on diode's forward voltage. Perform sufficient evaluation with actual application.
*2. $V_{\text {OUT(S) }}$ can be set by the ratio of $\mathrm{V}_{\mathrm{FB}}$ value and the output voltage setting resistors ( $\mathrm{R}_{\mathrm{FB} 1}, \mathrm{R}_{\mathrm{FB} 2}$ ). For details, refer to External Parts Selection".
*3. $\mathrm{V}_{\mathrm{FB}(\mathrm{S})}$ is a setting value for FB voltage.
*4. Power MOS FET ON resistance largely varies depending on the $\mathrm{V}_{\text {Out }}$ voltage.
*5. This is when the $\mathrm{V}_{\text {OUt }}$ voltage startups from the STU release voltage or more. The soft-start time largely varies depending on the load current and the input voltage when the S-8363 Series startups from the STU release voltage or less, because the S-8363 Series once enters the start-up mode. Refer to "■ 2. Low voltage start-up" for STU release voltage.

■ External Parts List When Measuring Electrical Characteristics
Table 6 External Parts List

| Element name | Symbol | Constants | Manufacturer | Part number |
| :--- | :---: | :---: | :---: | :---: |
| Inductor | L | $2.2 \mu \mathrm{H}$ | TDK Corporation | VLF302510 |
| Diode | SD | - | TOSHIBA CORPORATION | CRS08 |
| Input capacitor | $\mathrm{C}_{I N}$ | $1 \mu \mathrm{~F}$ | TAIYO YUDEN Co., Ltd. | EMK107B7105KA |
| Output capacitor | $\mathrm{C}_{\text {OUT }}$ | $10 \mu \mathrm{~F}$ | TAIYO YUDEN Co., Ltd. | LMK212BJ106KD |
| FB pin capacitor | $\mathrm{C}_{\mathrm{FB}}$ | 47 pF | TAIYO YUDEN Co., Ltd. | UMK105CH470JV |
| Output voltage setting resistor 1 | $\mathrm{R}_{\text {FB } 1}$ | $68 \mathrm{k} \Omega$ | ROHM Co., Ltd. | MCR03 series |
| Output voltage setting resistor 2 | $\mathrm{R}_{\mathrm{FB} 2}$ | $15 \mathrm{k} \Omega$ | ROHM Co., Ltd. | MCR03 series |

## Test Circuits

1. 



Figure 5
2.


Figure 6
3.


Figure 7

## Operation

## 1. Switching control method

The S-8363 Series switching regulator automatically switches between the pulse width modulation method (PWM) and pulse frequency modulation method (PFM) according to the load current.
A low ripple power can be supplied by operating on PWM control for which the pulse width changes up to $88 \%$ in the range where the output load current is large.
The S-8363 Series operates on PFM control when the output load current is small and the pulses are skipped according to the amount of the load current. Therefore, the oscillation circuit intermittently oscillates, reducing the self-current consumption. This prevents decrease in efficiency when the output load current is small. The ripple voltage during the PFM control is very small, so that the S-8363 Series realizes high efficiency and the low-noise power supply.
The point at which PWM control switches to PFM control varies depending on the external element (inductor, diode, etc.), input voltage value, and output voltage value, and this method achieves high efficiency in the output load current of about $100 \mu \mathrm{~A}$.

## 2. Low voltage start-up

## 2. 1 Start-up circuit

The S-8363 Series can startup from 0.9 V . When the Vout voltage at $\mathrm{ON} / \overline{\mathrm{OFF}}=$ " H " does not reach the STU release voltage, the start-up circuit starts the operation and outputs the fixed duty pulse to the CONT pin. By this, the Vout voltage starts step-up. After that, the Vout voltage reaches the STU release voltage and the STU mode circuit is set in STU release condition, therefore, the switching control circuit starts stable operation due to the soft-start function. Simultaneously, the start-up circuit is set in disable condition, so that the S-8363 Series prevents excessive current consumption.

## 2. 2 Start-up mode (STU mode) circuit

The STU mode circuit monitors the $\mathrm{V}_{\text {OUT }}$ voltage, and switches the operation modes between start-up period and normal control period of the switching control circuit. The STU release voltage is internally fixed at 1.4 V (typ.), and has hysteresis of approx. 0.15 V . When the $\mathrm{V}_{\text {out }}$ voltage decreases to 1.25 V (typ.) from release condition, the STU mode circuit is set in the STU detection condition, shifting to the start-up period. Several $\mu \mathrm{s}$ to several ten $\mu \mathrm{s}$ is taken to shift from STU release to PWM release. During this the step-up operation is not performed, therefore, the Vout voltage may largely decrease depending on the size of load.
During applying $\mathrm{ON} / \overline{\mathrm{OFF}}=$ " L ", the STU mode circuit is set in disable condition, so that the S-8363 Series prevents excessive current consumption.


Figure 8 Start-up Circuit


Figure 9 Start-up Sequence

## 2. 3 Schottky barrier diode

A schottky barrier diode (SD) is necessary to operate the S-8363 Series. The VOUT pin also works as the power supply pin. The voltage applied on the VOUT pin when $\mathrm{ON} / \overline{\mathrm{OFF}}=$ " L " is $\mathrm{V}_{\mathbb{I}}-\mathrm{V}_{\mathrm{D}} . \mathrm{V}_{\mathrm{D}}$ is forward voltage for step-down of SD, and largely varies depending on the forward current $I_{f}$ of SD and ambient temperature, but $\mathrm{V}_{\mathrm{d}}$ is approx. 0.2 V to 0.5 V .
When the S-8363 Series startups from 0.9 V , use a SD with specially low $\mathrm{V}_{\mathrm{D}}$. When using CRS08 for the S-8363 Series, start-up is guaranteed when $\mathrm{Ta}=+25^{\circ} \mathrm{C}$ and a load current of 1 mA .
Satisfy the following conditions when using other SDs.

- Low forward voltage (VD)
- High switching speed
- Reverse withstand voltage of $\mathrm{V}_{\text {OUT }}+$ spike voltage or more
- Rated current of lpK or more

Table 7 Typical Schottky Diodes

| Manufacturer | Name |
| :---: | :---: |
| TOSHIBA CORPORATION | CRS02 |
|  | CRS08 |
| ROHM Co., Ltd. | RB161M-20TR |
|  | RB051LA-40TR |
|  | RB070M-30TR |
|  | RB161SS-20T2R |

Remark Generally, in diodes with low forward volage $V_{D}$, reverse leakage current $I_{r}$ tends to increases. Especially, increase of $\mathrm{I}_{\mathrm{r}}$ in high temperature is significant. To prevent decrease in efficiency, choose a diode with low $\mathrm{I}_{\mathrm{r}}$ when low voltage start-up is unnecessary.

## 3. Soft-start function

The S-8363 Series has the built-in soft-start circuit. When power-on (connecting ON/ $\overline{\mathrm{OFF}}$ to $\mathrm{V}_{\text {IN }}$ ) or after start-up at $\mathrm{ON} / \overline{\mathrm{OFF}}=$ " H ", the output voltage $\left(\mathrm{V}_{\text {OUT }}\right)$ gradually rises, suppressing rush current and overshoot of the output voltage. In the S-8363 Series, the soft-start time ( $\mathrm{t}_{\mathrm{ss}}$ ) is from start-up to the time to reach $90 \%$ of the $V_{\text {OUt }}$ output voltage setting value ( $\mathrm{V}_{\text {OUT(S) }}$ ). A reference voltage adjustment method is adopted as the soft-start method, the reference voltage gradually rises from 0 V simultaneously with start of the soft-start. The soft-start circuit has two operation modes which is selected according to the $V_{\text {OUt }}$ voltage at start-up.

## $3.1 \mathrm{~V}_{\text {out }}$ voltage at start-up > STU release voltage

The soft-start starts when the reference voltage gradually rises after ON/ $\overline{\mathrm{OFF}}=$ " H ".


Figure 10

## 3. 2 V $_{\text {оut }}$ voltage at start-up < STU release voltage

After $\mathrm{ON} / \overline{\mathrm{OFF}}=$ " H ", step-up starts by the start-up operation. When the $\mathrm{V}_{\text {OUt }}$ voltage reaches the STU release voltage, the soft-start starts.
Since the length of the start-up period largely varies depending on the input voltage, load current, external parts and ambient temperature, the soft-start time varies according to them. Perform sufficient evaluation with actual application.


Figure 11

## 3. 3 Condition of performing soft-start again

The condition to reset after the reference voltage once rises (reference voltage from error amplifier $=0 \mathrm{~V}$ ) is to set the ON/ $\overline{\mathrm{OFF}}$ pin voltage to " L ". Setting $\mathrm{ON} / \overline{\mathrm{OFF}}=$ "H" starts soft-start again. When the Vout voltage drops and decreases more than the STU detection voltage by an overload, the soft-start circuit shifts to the start-up period. When the Vout voltage is restored by releasing overload, the soft-start function is performed.
If the $V_{\text {OUT }}$ voltage is not decreased less than the STU detection voltage, the soft-start function is not performed when restoration.


Figure 12 Reset Condition for Soft-Start

## 4. Power-off pin

This pin stops or starts step-up operations.
When the ON/ $\overline{\text { OFF }}$ pin is set to the low level, the internal driver of the CONT pin is turned off and all internal circuits stop substantially reducing the current consumption.
The ON/ $\overline{\text { OFF }}$ pin is set up as shown in Figure 13 and is internally pulled down by using the depression transistor, so all circuits stop even if this pin is floating. Do not apply a voltage of between 0.25 V and 0.75 V to the $\mathrm{ON} / \overline{\mathrm{OFF}}$ pin because applying such a voltage increases the current consumption. If the ON/ $\overline{\mathrm{OFF}}$ pin is not used, connect it to the VIN pin.

Table 8

| ON/ $\overline{\text { OFF }}$ pin | CR oscillation <br> circuit | Output voltage |
| :---: | :---: | :---: |
| "H" | Operates | Set value |
| "L" | Stops | $V_{\text {IN }}-V_{D}$ |



Figure 13

## 5. Current limit circuit

A current limit circuit is built in the S-8363 Series.
The current limit circuit monitors the current that flows in the Nch power MOS FET and limits current in order to prevent thermal destruction of the IC due to an overload or magnetic saturation of the inductor.
When a current exceeding the current limit detection value flows in the Nch power MOS FET, the current limit circuit operates and turns off the Nch power MOS FET since the current limit detection until one clock of the oscillator ends. The Nch power MOS FET is turned on in the next clock and the current limit circuit resumes current detection operation. If the value of the current that flows in the Nch power MOS FET remains the current limit detection value or more, the current limit circuit functions again and the same operation is repeated. Once the value of the current that flows in the Nch power MOS FET is lowered up to the specified value, the normal operation status restores.
The current limit detection value is fixed to 1.1 A (typ.) in the IC. However, under the condition that ON duty is small, between the detection delay time of the current limit circuit and the ON time of the Nch power MOS FET, the difference is small. Therefore, the current value which is actually limited is increased. Usually, when the difference between the VIN pin and VOUT pin is small, on duty is decreased and the limited current value is increased.

## Operation Principles

The S-8363 Series is a step-up switching regulator. Figure 14 shows the basic circuit diagram.
Step-up switching regulators start current supply by the input voltage $\left(\mathrm{V}_{\mathbb{I N}}\right)$ when the Nch power MOS FET is turned on and holds energy in the inductor at the same time. When the Nch power MOS FET is turned off, the CONT pin voltage is stepped up to discharge the energy held in the inductor and the current is discharged to Vout through the diode. When the discharged current is stored in Cout, a voltage is generated, and the potential of $\mathrm{V}_{\text {out }}$ increases until the voltage of the FB pin reaches the same potential as the internal reference voltage.
For the PWM control method, the switching frequency (fosc) is fixed and the Vout voltage is held constant according to the ratio of the ON time and OFF time (ON duty) of the Nch power MOS FET in each period.
In the PWM control method, the Vout voltage is held constant by controlling the ON time.
In the PFM control method, the Nch power MOS FET is turned on by fixed duty. When energy is discharged to Vout once and the Vout potential exceeds the set value, the Nch power MOS FET stays in the off status until $V_{\text {out }}$ decreases to the set value or less due to the load discharge. Time $V_{\text {OUT }}$ decreases to the set value or less depends on the amount of load current, so, the switching frequency varies depending on this current.


Figure 14 Basic Circuit of Step-up Switching Regulator
The ON duty in the current continuous mode can be calculated by using the equation below. Use the S-8363 Series in the range where the ON duty is less than the maximum duty.
The maximum duty is $88 \%$ (typ.).

ON duty $=\left(1-\frac{V_{\text {IN }}}{V_{\text {OUT }}+V_{D}{ }^{\text {T1 }}}\right) \times 100[\%]$
*1. $V_{D}$ : Forward voltage of diode

## 1. Continuous current mode

The following explains the current that flows into the inductor when the step-up operation stabilizes in a certain status and lout is sufficiently large.
When the Nch power MOS FET is turned on, current $\left(\mathrm{I}_{1}\right)$ flows in the direction shown in Figure 14. The inductor current ( $\mathrm{I}_{\mathrm{L}}$ ) at this time gradually increases in proportion with the ON time ( $\mathrm{t}_{\mathrm{N}}$ ) of the Nch power MOS FET, as shown in Figure 15.

Current change of inductor within $t_{\text {ON }}$ :

$$
\begin{aligned}
\Delta I_{\mathrm{LON})} & =I_{L} \max .-I_{\mathrm{L}} \min . \\
& =\frac{\mathrm{V}_{\mathrm{IN}}}{\mathrm{~L}} \times \mathrm{t}_{\mathrm{ON}}
\end{aligned}
$$

When the Nch power MOS FET is turned off, the voltage of the CONT pin is stepped up to $V_{o u t}+V_{D}$ and the voltage on both ends of the inductor becomes $V_{\text {OUT }}+V_{D}-V_{\text {IN }}$. However, it is assumed here that $V_{\text {OUT }} \gg V_{D}$ and $V_{D}$ is ignored.

## Current change of inductor within toff :

$$
\Delta \mathrm{L}_{\mathrm{L}(\text { OFF })}=\frac{\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}}{\mathrm{L}} \times \mathrm{t}_{\text {OFF }}
$$

The input power equals the output power in an ideal situation where there is no loss by components.

$$
\begin{align*}
& I_{\text {IN(AV) }}: \\
& P_{\text {IN }}=P_{\text {OUT }} \\
& I_{\text {IN }(A V)} \times V_{\text {IN }}=I_{\text {OUT }} \times V_{\text {OUT }} \\
& \therefore I_{\text {IN }(A V)}=\frac{V_{\text {OUT }}}{V_{\text {IN }}} \times \operatorname{loUT} . \tag{1}
\end{align*}
$$

The current that flows in the inductor consists of a ripple current that changes due to variation over time and a direct current.

## From Figure 15 :

$I_{\operatorname{IN}(A V)}$ :

$$
\begin{align*}
\operatorname{I}_{\operatorname{IN}(A V)} & =I_{\operatorname{IN(DC)}}+\frac{\Delta \mathrm{I}_{\mathrm{L}}}{2} \\
& =\mathrm{I}_{\operatorname{IN(DC)}}+\frac{\mathrm{V}_{\text {OUT }}-\mathrm{V}_{\text {IN }}}{2 \times \mathrm{L}} \times \mathrm{t}_{\text {OFF }} \\
& =\operatorname{I}_{\operatorname{IN}(\mathrm{DC})}+\frac{\mathrm{V}_{\text {IN }}}{2 \times \mathrm{L}} \times \mathrm{t}_{\mathrm{ON}} \ldots \ldots \ldots \ldots . . \tag{2}
\end{align*}
$$

Above, the continuous mode is the operation mode when $\operatorname{liN(DC)}>0$ as shown in Figure 15 and the inductor current continuously flows.
While the output current (lout) continues to decrease, $\mathrm{I}_{\mathbb{N}(\mathrm{DC})}$ reaches 0 as shown in Figure 16. This point is the critical point of the continuous mode.
As shown in equations (1) and (2), the direct current component (lin(DC)) depends on lout.
$\mathrm{I}_{\text {OUt(0) }}$ when $\mathrm{I}_{\mathrm{IN}(\mathrm{DC})}$ reaches 0 (critical point):

$$
\mathrm{I}_{\text {OUT(0) }}=\frac{\mathrm{t}_{\text {ON }} \times \mathrm{V}_{\text {IN }}{ }^{2}}{2 \times \mathrm{L} \times \mathrm{V}_{\text {OUT }}}
$$

When the output current decreases below $\mathrm{l}_{\text {OUt(0) }}$, the current flowing in the inductor stops flowing in the $\mathrm{t}_{\mathrm{ffF}}$ period as shown in Figure 17. This is the discontinuous mode.


Figure 15 Continuous Mode (Current Cycle of Inductor Current $\mathrm{I}_{\mathrm{L}}$ )


Figure 16 Critical Point (Current Cycle of Inductor Current $\mathrm{I}_{\mathrm{L}}$ )


Figure 17 Discontinuous Mode (Current Cycle of Inductor Current $\mathrm{I}_{\mathrm{L}}$ )

## ■ External Parts Selection

## 1. Inductor

The recommended $L$ value of the $\mathrm{S}-8363$ Series is $2.2 \mu \mathrm{H}$.
Caution When selecting an inductor, be careful about its allowable current. If a current exceeding the allowable current flows through the inductor, magnetic saturation occurs, substantially lowering the efficiency and destroying ICs due to large current. Therefore, select an inductor such that lpK does not exceed the allowable current. The following equations express $I_{\text {PK }}$ in the ideal statuses in the discontinuous and continuous modes :

$$
\begin{array}{ll}
I_{\text {PK }}=\sqrt{\frac{2 \times I_{\text {OUT }} \times\left(V_{\text {OUT }}+V_{D}{ }^{* 2}-V_{\text {IN }}\right)}{f_{\text {OSSC }}{ }^{* 1} \times L}} & \text { (Discontinuous mode) } \\
I_{\text {PK }}=\frac{V_{\text {OUT }}+V_{D}{ }^{* 2}}{V_{\text {IN }}} \times I_{\text {OUT }}+\frac{\left(V_{\text {OUT }}+V_{D}{ }^{* 2}-V_{\text {IN }}\right) \times V_{\text {IN }}}{2 \times\left(V_{\text {OUT }}+V_{D}{ }^{* 2}\right) \times f_{\text {OSC }}{ }^{* 1} \times L} & \text { (Continuous mode) }
\end{array}
$$

*1. fosc : oscillation frequency
*2. $V_{D}$ is the forward voltage of a diode. The reference value is 0.4 V . However, current exceeding the above equation flows because conditions are practically not ideal. Perform sufficient evaluation with actual application.

Table 9 Typical Inductors

| Manufacturer | Name | $\underline{L}$ value | Direct resistor | Rated current | Size $(\mathrm{L} \times \mathrm{W} \times \mathrm{H})$ [mm] |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TDK Corporation | VLF302510-2R2M | $2.2 \mu \mathrm{H}$ | $0.084 \Omega$ max. | 1.23 A max. | $3.0 \times 2.5 \times 1.0$ |
|  | VLS3010T-2R2M | $2.2 \mu \mathrm{H}$ | $0.116 \Omega$ max. | 1.2 A max. | $3.0 \times 3.0 \times 1.0$ |
|  | VLS201610E | $2.2 \mu \mathrm{H}$ | $0.276 \Omega$ max. | 0.94 A max. | $2.0 \times 1.6 \times 0.95$ |
|  | MLP2012S2R2M | $2.2 \mu \mathrm{H}$ | $0.300 \Omega$ max. | 0.8 A max. | $2.0 \times 1.25 \times 1.0$ |
| Coilcraft, Inc | LPS3010-222ML | $2.2 \mu \mathrm{H}$ | $0.220 \Omega$ max. | 1.3 A max. | $3.0 \times 3.0 \times 1.0$ |
| Murata Manufacturing Co., Ltd. | LQM2HPN2R2MG0 | $2.2 \mu \mathrm{H}$ | $0.080 \Omega \pm 25 \%$ | 1.3 A max. | $2.5 \times 2.0 \times 1.0$ |
|  | LQH3NPN2R2NG0 | $2.2 \mu \mathrm{H}$ | $0.140 \Omega \pm 20 \%$ | 1.25 A max. | $2.7 \times 3.0 \times 1.0$ |
| TAIYO YUDEN Co., Ltd. | NR3010T2R2M | $2.2 \mu \mathrm{H}$ | $0.114 \Omega$ max. | 1.1 A max. | $3.0 \times 3.0 \times 1.0$ |
|  | NR4010T2R2N | $2.2 \mu \mathrm{H}$ | $0.180 \Omega$ max. | 1.15 A max. | $4.0 \times 4.0 \times 1.0$ |
|  | BRL2518T2R2M | $2.2 \mu \mathrm{H}$ | $0.1755 \Omega$ max. | 0.85 A max. | $2.5 \times 1.8 \times 1.2$ |

## 2. Diode

Use an externally mounted that meets the following conditions.

- Low forward voltage (Schottky barrier diode or similar types)
- High switching speed
- Reverse withstand voltage of $\mathrm{V}_{\text {OUT }}+$ spike voltage or more
- Rated current of l l


## 3. Input capacitor ( $\mathrm{C}_{\mathrm{IN}}$ ) and output capacitor ( $\mathrm{C}_{\text {оит }}$ )

To improve efficiency, an input capacitor ( $\mathrm{C}_{\mathrm{IN}}$ ) lowers the power supply impedance and averages the input current. Select $\mathrm{C}_{\mathrm{IN}}$ according to the impedance of the power supply used. The recommended capacitance is $1 \mu \mathrm{~F}$ or more for the S-8363 Series.
An output capacitor (Соит), which is used to smooth the output voltage, requires a capacitance larger than that of the step-down type because the current is intermittently supplied from the input to the output side in the step-up type. When the output voltage is low or the load current is large, enlarging an output capacitance value is required. Moreover, when the output voltage is high, connecting a $0.1 \mu \mathrm{~F}$ ceramic capacitor in parallel is required. Mount near a VOUT pin as possible.
The indication of an output capacitor to the setting value of $\mathrm{V}_{\text {out }}$ voltage is shown in the table 10. Perform thorough evaluation using an actual application to set the constant when selecting parts.
A ceramic capacitor can be used for both the input and output.

Table 10 Recommended Output Capacitance

| V Out voltage | Output capacitor (Cout) |
| :---: | :---: |
| $<2.5 \mathrm{~V}$ | $10 \mu \mathrm{~F} \times 2$ |
| 2.5 V to 4.0 V | $10 \mu \mathrm{~F}$ |
| $4.0 \mathrm{~V}<$ | $10 \mu \mathrm{~F}+0.1 \mu \mathrm{~F}$ |

## 4. Output voltage setting resistors ( $\mathrm{R}_{\mathrm{FB} 1}, \mathrm{R}_{\mathrm{FB} 2}$ ), capacitor for phase compensation ( $\mathrm{C}_{\mathrm{FB}}$ )

For the S-8363 Series, Vout can be set to any value by using external divider resistors. Connect the divider resistors between the VOUT and VSS pins.
Because $\mathrm{V}_{\mathrm{FB}}=0.6 \mathrm{~V}$ typ., $\mathrm{V}_{\text {Out }}$ can be calculated by using the following equation :

$$
V_{\text {OUT }}=\frac{R_{F B 1}+R_{F B 2}}{R_{F B 2}} \times 0.6
$$

Connect divider resistors $\mathrm{R}_{\text {FB1 }}$ and $\mathrm{R}_{\text {FB2 }}$ as close to the IC as possible to minimize the effects of noise. If noise has an effect, adjust the values of $R_{F B 1}$ and $R_{F B 2}$ so that $R_{F B 1}+R_{F B 2}<100 \mathrm{k} \Omega$.
$C_{F B}$, which is connected in parallel with $R_{F B 1}$, is a capacitor for phase compensation.
By setting the zero point (the phase feedback) by adding capacitor $\mathrm{C}_{\mathrm{FB}}$ to output voltage setting resistor $\mathrm{R}_{\mathrm{FB} 1}$ in parallel, the phase margin increases, improving the stability of the feedback loop. To effectively use the feedback portion of the phase based on the zero point, define $\mathrm{C}_{\mathrm{FB}}$ by using the following equation :

$$
C_{F B} \cong \frac{\sqrt{L \times C_{O U T}}}{3 \times R_{F B 1}} \times \frac{V_{O U T}}{V_{D D}}
$$

This equation is only a guide.
The following explains the optimum setting.
To efficiently use the feedback portion of the phase based on the zero point, specify settings so that the phase feeds back at the zero point frequency ( $\mathrm{f}_{\text {zero }}$ ) of $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{C}_{\mathrm{FB}}$ according to the phase delay at the pole frequency ( $\mathrm{f}_{\text {pole }}$ ) of $L$ and $\mathrm{C}_{\text {out }}$. The zero point frequency is generally set slightly higher than the pole frequency.
The following equations are used to determine the pole frequency of $L$ and $C_{o u t}$ and the zero point frequency set using $\mathrm{R}_{\mathrm{FB} 1}$ and $\mathrm{C}_{\mathrm{FB}}$.

$$
\begin{aligned}
& \mathrm{f}_{\text {pole }} \cong \frac{1}{2 \times \pi \times \sqrt{\mathrm{L} \times \mathrm{C}_{\mathrm{OUT}}}} \times \frac{\mathrm{V}_{\mathrm{DD}}}{\mathrm{~V}_{\mathrm{OUT}}} \\
& \mathrm{f}_{\mathrm{zero}} \cong \frac{1}{2 \times \pi \times \mathrm{R}_{\mathrm{FB} 1} \times \mathrm{C}_{\mathrm{FB}}}
\end{aligned}
$$

The transient response can be improved by setting the zero point frequency in a lower frequency range. If, however, the zero point frequency is set in a significantly lower range, the gain increases in the range of high frequency and the phase margin decreases. This might result in unstable operation. Determine the proper value after sufficient evaluation with actual application.

The typical constants based on our evaluation are shown in Table 11.

Table 11 Example of Constant for External Parts

| $\mathrm{V}_{\text {OUT(S) }}[\mathrm{V}]$ | $\mathrm{V}_{\text {IN }}[\mathrm{V}]$ | $\mathrm{R}_{\mathrm{FB} 1}[\mathrm{k} \Omega]$ | $\mathrm{R}_{\mathrm{FB} 2}[\mathrm{k} \Omega]$ | $\mathrm{C}_{\mathrm{FB}}[\mathrm{pF}]$ |
| :---: | :---: | :---: | :---: | :---: |
| 1.8 | 1.2 | 30 | 15 | 82 |
| 2.48 | 1.2 | 47 | 15 | 68 |
| 3.32 | 1.8 | 68 | 15 | 47 |
| 4.2 | 1.8 | 90 | 15 | 39 |
| 5.0 | 1.8 | 110 | 15 | 39 |

## ■ Standard Circuit



Figure 18
Caution The above connection diagram and constant will not guarantee successful operation. Perform thorough evaluation using an actual application to set the constants.

## ■ Precaution

- Mount external capacitors and inductor as close as possible to the IC. Set single point ground.
- Characteristics ripple voltage and spike noise occur in IC containing switching regulators. Moreover rush current flows at the time of a power supply injection. Because these largely depend on the inductor, the capacitor and impedance of power supply used, perform sufficient evaluation with actual application.
- The $0.1 \mu \mathrm{~F}$ capacitor connected between the VOUT and VSS pins is a bypass capacitor. It stabilizes the power supply in the IC when application is used with a heavy load, and thus effectively works for stable switching regulator operation. Allocate the bypass capacitor as close to the IC as possible, prioritized over other parts.
- Although the IC contains a static electricity protection circuit, static electricity or voltage that exceeds the limit of the protection circuit should not be applied.
- The power dissipation of the IC greatly varies depending on the size and material of the board to be connected. Perform sufficient evaluation using an actual application before designing.
- ABLIC Inc. claims no responsibility for any disputes arising out of or in connection with any infringement by products including this IC of patents owned by a third party.


## Application Circuits

Application circuits are examples. They may always not guarantee successful operation.

## 1. External parts for application circuits

Table 12 Characteristics of External Parts

| Part | Part Name | Manfuacturer | Characteristics |
| :---: | :---: | :---: | :---: |
| Inductor | VLF302510 | TDK Corporation | $\begin{aligned} & 2.2 \mu \mathrm{H}, \mathrm{DCR}^{* 1}=0.084 \Omega, \mathrm{I}_{\mathrm{MAX}}{ }^{* 2}=1.23 \mathrm{~A}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=3.0 \times 2.5 \times 1.0 \mathrm{~mm} \end{aligned}$ |
|  | VLS201610E |  | $2.2 \mu \mathrm{H}, \mathrm{DCR}^{* 1}=0.276 \Omega, \mathrm{I}_{\mathrm{MAX}}{ }^{* 2}=0.94 \mathrm{~A}$, <br> $\mathrm{L} \times \mathrm{W} \times \mathrm{H}=2.0 \times 1.6 \times 0.95 \mathrm{~mm}$ |
|  | MLP2012S |  | $\begin{aligned} & 2.2 \mu \mathrm{H}, \mathrm{DCR}^{* 1}=0.300 \Omega, \mathrm{I}_{\mathrm{MAX}}{ }^{* 2}=0.8 \mathrm{~A}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=2.0 \times 1.25 \times 1.0 \mathrm{~mm} \end{aligned}$ |
|  | BRL2518T2R2M | TAIYO YUDEN Co., Ltd. | $\begin{aligned} & 2.2 \mu \mathrm{H}, \mathrm{DCR}^{* 1}=0.1755 \Omega, \mathrm{I}_{\mathrm{MAX}}^{*_{2}}=0.85 \mathrm{~A}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=2.5 \times 1.8 \times 1.2 \mathrm{~mm} \end{aligned}$ |
| Diode | CRS02 | TOSHIBA CORPORATION | $\begin{aligned} & V_{F}{ }^{* 3}=0.4 \mathrm{~V} \text { typ., } \mathrm{I}_{\mathrm{F}}^{{ }^{* 4}}=1.0 \mathrm{~A}, \mathrm{~V}_{R}^{{ }^{*} 5}=30 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=3.5 \times 1.6 \times 1.08 \mathrm{~mm} \end{aligned}$ |
|  | CRS08 |  | $\begin{aligned} & \mathrm{VF}_{F}^{* 3}=0.32 \mathrm{~V} \text { typ., } \mathrm{IF}_{\mathrm{F}}{ }^{44}=1.5 \mathrm{~A}, \mathrm{~V}_{R}{ }^{{ }^{5} 5}=30 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=3.5 \times 1.6 \times 1.08 \mathrm{~mm} \end{aligned}$ |
|  | RB070M-30TR | ROHM Co., Ltd. | $\begin{aligned} & \mathrm{V}_{F}^{{ }^{3}}=0.44 \mathrm{~V} \text { typ., } \mathrm{IF}_{\mathrm{F}}{ }^{4}=1.5 \mathrm{~A}, \mathrm{~V}_{R}{ }^{{ }^{5}}=30 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=3.5 \times 1.6 \times 0.9 \mathrm{~mm} \end{aligned}$ |
|  | RB051LA-40TR |  | $\begin{aligned} & V_{F}{ }^{* 3}=0.35 \mathrm{~V} \text { max., }, \mathrm{I}_{\mathrm{F}}{ }^{* 4}=3.0 \mathrm{~A}, \mathrm{~V}_{R}{ }^{*} 5=20 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=4.7 \times 2.6 \times 1.05 \mathrm{~mm} \end{aligned}$ |
|  | RB161M-20TR |  | $\mathrm{V}_{\mathrm{F}}^{* 3}=0.31 \mathrm{~V} \text { typ., } \mathrm{IF}_{\mathrm{F}}{ }^{* 4}=1.0 \mathrm{~A}, \mathrm{~V}_{\mathrm{R}}{ }^{{ }^{5}}=20 \mathrm{~V},$ |
|  | RB161SS-20T2R |  | $\begin{aligned} & V_{F}{ }^{{ }^{3}}=0.42 \mathrm{~V}, \mathrm{I}_{\mathrm{F}}^{{ }^{4}}=3.0 \mathrm{~A}, \mathrm{~V}_{\mathrm{R}}^{{ }^{* 5}}=20 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=1.6 \times 0.8 \times 0.603 \mathrm{~mm} \end{aligned}$ |
| Capacitor | LMK212BJ106KD | TAIYO YUDEN Co., Ltd. | $\begin{aligned} & 10 \mu \mathrm{~F}, \mathrm{E}_{\mathrm{DC}}{ }^{{ }^{6}}=10 \mathrm{~V}, \mathrm{X} 5 \mathrm{R}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=2.0 \times 1.25 \times 0.95 \mathrm{~mm} \end{aligned}$ |
|  | EMK107B7105KA |  | $\begin{aligned} & 10 \mu \mathrm{~F}, \mathrm{E}_{\mathrm{DC}}{ }^{{ }^{6} 6}=16 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=1.6 \times 0.8 \times 0.90 \mathrm{~mm} \end{aligned}$ |
|  | C1608X5R0J106M | TDK Corporation | $\begin{aligned} & 10 \mu \mathrm{~F}, \mathrm{E}_{\mathrm{DC}}{ }^{*}{ }^{6}=6.3 \mathrm{~V}, \mathrm{X} 5 \mathrm{R}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=1.6 \times 0.8 \times 0.9 \mathrm{~mm} \end{aligned}$ |
|  | C1608X7R1C105K |  | $\begin{aligned} & 1 \mu \mathrm{~F}, \mathrm{E}_{\mathrm{DC}}{ }^{* 6}=16 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=1.6 \times 0.8 \times 0.9 \mathrm{~mm} \end{aligned}$ |

* 1. DCR: DC resistance
*2. $I_{\text {max }}$ : Maximum allowable current
* 3. $V_{F}$ : Forward voltage
* 4. $I_{F}$ : Forward current
* 5. $\mathrm{V}_{\mathrm{R}}$ : Reverse voltage
* 6. EDC: Rated voltage


## 2. A power supply started by 0.9 V

Following shows a power supply example which starts up by using the final voltage ( 0.9 V ) of dry cells and its characteristics.


Figure 19 Circuit Example (For a power supply started by 0.9 V )

Table 13 External Parts Examples (For a power supply started by 0.9 V)

| Condition | Output <br> Voltage | IC Product <br> Name | L Product <br> Name | SD Product <br> Name | Cout Product Name | $R_{F B 1}$ | $R_{F B 2}$ | $\mathrm{C}_{\mathrm{FB}}$ |
| :---: | :---: | :---: | :---: | :--- | :--- | :--- | :--- | :--- |
| 1 | 3.3 V | S-8363B | VLF302510 | RB161M-20TR | LMK212BJ106KD | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 2 | 3.3 V | S-8363B | VLF302510 | RB051LA-40TR | LMK212BJ106KD | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 3 | 3.3 V | S-8363B | VLF302510 | RB070M-30TR | LMK212BJ106KD | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 4 | 3.3 V | S-8363B | VLF302510 | RB161SS-20T2R | LMK212BJ106KD | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 5 | 3.3 V | S-8363B | VLF302510 | CRS02 | LMK212BJ106KD | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 6 | 3.3 V | S-8363B | VLF302510 | CRS08 | LMK212BJ106KD | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |

Caution The above connection will not guarantee successful operation. Perform thorough evaluation using an actual application to set the constant.

## 3. Output characteristics of power supply started by 0.9 V

Following shows the (1) Load current (lout) vs. Operating start voltage ( $\mathrm{V}_{\mathrm{ST}}$ ), (2) Temperature ( Ta ) vs. Operating start voltage ( $\mathrm{V}_{\text {ST }}$ ), (3) Load current (lout) vs. Efficiency ( $\eta$ ), (4) Load current (lout) vs. Output voltage (VOUT), characteristics for conditions 1 to 6 in Table 13.


## 4. Super-small power supply

Following shows a circuit example which gives top priority to reduce the implementation area by using the small external parts and its characteristics.


Figure 20 Circuit Example (For super-small power supply)

Table 14 External Parts Examples (For super-small power supply)

| Condition | Output <br> Voltage | IC Product <br> Name | L Product <br> Name | SD Product Name | Cout1 | Cout2 | $\mathrm{R}_{\mathrm{FB} 1}$ | $\mathrm{R}_{\text {FB2 }}$ | $\mathrm{C}_{\text {FB }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.8 V | S-8363B | MLP2012S | RB161SS-20 | C1608X5R0J106M | C1608X5R0J106M | $30 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 82 pF |
| 2 | 3.3 V | S-8363B | MLP2012S | RB161SS-20 | LMK212BJ106KD | $0.1 \mu \mathrm{~F}$ | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 3 | 1.8 V | S-8363B | VLS201610E | RB161SS-20 | C1608X5R0J106M | C1608X5R0J106M | $30 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 82 pF |
| 4 | 3.3 V | S-8363B | VLS201610E | RB161SS-20 | LMK212BJ106KD | $0.1 \mu \mathrm{~F}$ | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 5 | 1.8 V | S-8363B | BRL2518T2R2M | RB161SS-20 | C1608X5R0J106M | C1608X5R0J106M | $30 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 82 pF |
| 6 | 3.3 V | S-8363B | BRL2518T2R2M | RB161SS-20 | LMK212BJ106KD | $0.1 \mu \mathrm{~F}$ | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |

Caution The above connection will not guarantee successful operation. Perform thorough evaluation using an actual application to set the constant.

## 5. Output characteristics of super-small power supply

Following shows the output current (lout) vs. efficiency ( $\eta$ ), output current (lout) vs. output voltage ( $\mathrm{V}_{\text {OUT }}$ ), and output current (lout) vs. ripple voltage ( $\mathrm{V}_{\mathrm{r}}$ ) characteristics for conditions 1 to 6 in Table 14.

## Condition 1





## Condition 2





## Condition 3





## Condition 4





## Condition 5





## Condition 6





## ■ Characteristics (Typical Data)

## 1. Examples of Major Power Supply Dependence Characteristics ( $\mathrm{Ta}=+\mathbf{2 5}{ }^{\circ} \mathrm{C}$ )

(1) Current consumption during operation ( $l_{\mathrm{l}_{1} 1}$ ) vs.

Operating input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )
Current consumption during switching off ( $l_{\mathrm{I}_{2} 2}$ ) vs.
Operating input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

(2) Current consumption during operation ( $\mathrm{I}_{\mathrm{ss} 1}$ ) vs. Output voltage ( $\mathrm{V}_{\text {out }}$ )
Current consumption during switching off ( $\mathrm{I}_{\mathrm{ss} 2}$ ) vs. Output voltage ( $\mathrm{V}_{\text {out }}$ )

(3) Current consumption during power-off ( $\mathrm{I}_{\text {sss }}$ ) vs. Operating input voltage ( $\mathrm{V}_{\text {IN }}$ ), Output voltage ( $\mathrm{V}_{\text {OUT }}$ )

(4) Oscillation frequency ( $f_{o s c}$ ) vs.

Output voltage (Vout)

(6) Maximum duty ratio (MaxDuty) vs.

Output voltage ( $\mathrm{V}_{\text {out }}$ )


(7) Soft-start time ( $\mathrm{t}_{\mathrm{ss}}$ ) vs. Output voltage ( $\mathrm{V}_{\text {out }}$ )

(8) PWM / PFM switching duty ratio (PFMDuty) vs. Operating input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

(10) Limited current (luig) vs.

Operating input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

(12) Power MOS FET leakage current (llsw) vs. Output voltage (Vout)

(14) Low level input voltage ( $\mathrm{V}_{\text {sL }}$ ) vs.

Operating input voltage ( $\mathrm{V}_{\text {IN }}$ )

(9) Output current at PWM / PFM switching (IPFM) vs. Operating input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

(11) Maximum load current (loutmax) vs.

Operating input voltage ( $\mathrm{V}_{\mathrm{IN}}$ )

(13) High level input voltage ( $\mathrm{V}_{\text {SH }}$ ) vs.

(15) FB voltage ( $\mathrm{V}_{\mathrm{FB}}$ ) vs. Output voltage ( $\mathrm{V}_{\mathrm{OUT}}$ )


## 2. Examples of Major Temperature Characteristics ( $\mathrm{Ta}=-40$ to $+85^{\circ} \mathrm{C}$ )

(1) Current consumption during operation (liN1) vs.

Temperature ( Ta )

(2) Current consumption during operation ( $\mathrm{I}_{\mathrm{ss} 1}$ ) vs.

Temperature (Ta)
(3) Current consumption during switching off (lin2) vs. Temperature ( Ta )

(4) Current consumption during switching off (Iss2) vs. Temperature (Ta)

(5) Current consumption during power-off (Isss) vs. Temperature (Ta)

(6) Oscillation frequency (fosc) vs. Temperature ( $\mathbf{T a}$

(7) Start-up oscillation frequency ( $\mathrm{f}_{\mathrm{ST}}$ ) vs. Temperature ( Ta )

(8) Maximum duty ratio (MaxDuty) vs. Temperature (Ta)

(10) PWM / PFM switching duty ratio (PFMDuty) vs.

(12) Limited current (lıim) vs.

Temperature ( Ta )

(14) Power MOS FET leakage current (lısw) vs.

Temperature ( Ta )

(9) Soft-start time (tss) vs. Temperature (Ta)

(11) Output current at PWM / PFM switching (IPFM) vs. Temperature ( Ta )

(13) Maximum load current (loutmax) vs.

Temperature ( Ta )

(15) High level input voltage ( $\mathrm{V}_{\mathrm{SH}}$ ) vs.

Temperature (Ta)

(16) Low level input voltage ( $\mathrm{V}_{\mathrm{SL}}$ ) vs Temperature ( Ta )

(18) Operating start voltage $\left(\mathbf{V}_{\mathrm{ST}}\right)$ vs.

Temperature (Ta)

(17) FB voltage ( $\mathrm{V}_{\mathrm{FB}}$ ) vs. Temperature ( Ta )

(19) Start-up mode release voltage ( $\mathrm{V}_{\text {stu+ }}$ ) vs.


## 3. Output waveform

(1)
$\mathrm{V}_{\text {OUT }}=3.3 \mathrm{~V}\left(\mathrm{~V}_{\text {IN }}=1.98 \mathrm{~V}\right)$


(2) $\mathrm{V}_{\text {OUT }}=5.0 \mathrm{~V}\left(\mathrm{~V}_{\text {IN }}=3.0 \mathrm{~V}\right)$



$-2.0$





## 4. Examples of Transient Response Characteristics

Unless otherwise specified, the used parts are those in Table 6 External Parts List.
4.1 At power-on ( $\mathrm{V}_{\mathrm{OUT}(\mathrm{S})}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=0 \mathrm{~V} \rightarrow \mathbf{0 . 9} \mathrm{~V}$, $\mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

4.2 At power-on ( $\mathrm{V}_{\text {Out( } \mathrm{S})}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=\mathbf{0 V} \rightarrow \mathbf{2 . 0} \mathrm{V}$, $\mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

4.3 Power-off pin response ( $\mathrm{V}_{\mathrm{OUT}}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=0.9 \mathrm{~V}, \mathrm{~V}_{\text {ON/OFF }}=0 \mathrm{~V} \rightarrow 0.9 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )
(1) $\mathrm{l}_{\text {OUt }}=1 \mathrm{~mA}$

4.4 Power-off pin response ( $\mathrm{V}_{\text {OUT }}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=2.0 \mathrm{~V}, \mathrm{~V}_{\text {ON/OFF }}=0 \mathrm{~V} \rightarrow 2.0 \mathrm{~V}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

4.5 Power supply voltage fluctuations ( $\mathrm{V}_{\text {OUT }}=3.0 \mathrm{~V}$, $\mathrm{I}_{\text {OUT }}=100 \mathrm{~mA}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

(2) $\mathrm{V}_{\mathrm{IN}}=2.64 \mathrm{~V} \rightarrow 1.98 \mathrm{~V}$


4.6 Load fluctuations ( $\mathrm{V}_{\text {OUT }}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=1.98 \mathrm{~V}$, I lout $=0.1 \mathrm{~mA} \rightarrow 100 \mathrm{~mA} \rightarrow 0.1 \mathrm{~mA}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )

4.7 Load fluctuations ( $\mathrm{V}_{\text {OUT }}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}=1.98 \mathrm{~V}$, $\mathrm{I}_{\text {OUT }}=100 \mathrm{~mA} \rightarrow 200 \mathrm{~mA} \rightarrow 100 \mathrm{~mA}, \mathrm{Ta}=+25^{\circ} \mathrm{C}$ )


STEP-UP, SUPER-SMALL PACKAGE, 1.2 MHz PWM/PFM SWITCHABLE SWITCHING REGULATOR

## ■ Reference Data

Reference data is provided to determine specific external components. Therefore, the following data shows the characteristics of the recommended external components selected for various applications.

## 1. External parts

Table 15 Efficiency vs. Output Current Characteristics and Output Voltage vs. Output Current Characteristics for External Parts (1/2)

| Condition | Product Name | Output Voltage | L Product Name | SD Product Name | Clin $^{\text {In }}$ |
| :---: | :--- | :---: | :--- | :--- | :--- |
| 1 | S-8363B | 1.8 V | VLF302510 | CRS08 | C1608X7R1C105K |
| 2 | S-8363B | 3.3 V | VLF302510 | CRS08 | EMK107B7105KA |
| 3 | S-8363B | 5.0 V | VLF302510 | CRS08 | EMK107B7105KA |
| 4 | S-8363B | 3.3 V | VLF302510 | CRS08 | C1608X7R1C105K |
| 5 | S-8363B | 3.3 V | VLF302510 | CRS08 | C1608X7R1C105K |
| 6 | S-8363B | 3.3 V | VLF302510 | RB070M-30TR | EMK107B7105KA |
| 7 | S-8363B | 3.3 V | VLF302510 | RB051LA-40TR | EMK107B7105KA |

Table 15 Efficiency vs. Output Current Characteristics and Output Voltage vs. Output Current Characteristics for External Parts (2 / 2)

| Condition | Cout1 $^{\|c\|}$ Cout2 $^{\prime}$ | Cout3 | $\mathrm{R}_{\text {FB1 }}$ | $\mathrm{R}_{\text {FB2 }}$ | $\mathrm{C}_{\text {FB }}$ |  |
| :---: | :--- | :--- | :--- | :---: | :---: | :---: |
| 1 | C1608X5R0J106M | C1608X5R0J106M | - | $30 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 82 pF |
| 2 | LMK212BJ106KD | $0.1 \mu \mathrm{~F}$ | - | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 3 | LMK212BJ106KD | $0.1 \mu \mathrm{~F}$ | - | $110 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 38 pF |
| 4 | C1608X5R0J106M | C1608X5R0J106M | - | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 5 | C1608X5R0J106M | C1608X5R0J106M | C1608X5R0J106M | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 6 | LMK212BJ106KD | $0.1 \mu \mathrm{~F}$ | - | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |
| 7 | LMK212BJ106KD | $0.1 \mu \mathrm{~F}$ | - | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | 47 pF |

The properties of the external parts are shown below.
Table 16 Characteristics of External Parts

| Part | Part Name | Manfuacturer | Characteristics |
| :---: | :---: | :---: | :---: |
| Inductor | VLF302510 | TDK Corporation | $\begin{aligned} & 2.2 \mu \mathrm{H}, \mathrm{DCR}^{* 1}=0.084 \Omega, \mathrm{I}_{\mathrm{MAX}}{ }^{* 2}=1.23 \mathrm{~A}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=3.0 \times 2.5 \times 1.0 \mathrm{~mm} \end{aligned}$ |
| Diode | CRS08 | TOSHIBA CORPORATION | $\begin{aligned} & \mathrm{V}_{F}^{{ }^{*}}=0.32 \mathrm{~V} \text { typ., } \mathrm{I}_{\mathrm{F}}^{{ }^{* 4}}=1.5 \mathrm{~A}, \mathrm{~V}_{R}^{{ }^{{ }^{5} 5}}=30 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=3.5 \times 1.6 \times 1.08 \mathrm{~mm} \end{aligned}$ |
|  | RB070M-30TR | ROHM Co., Ltd. | $\begin{aligned} & \mathrm{V}_{F}^{{ }^{3}}=0.44 \mathrm{~V} \text { typ., } \mathrm{I}_{\mathrm{F}}^{{ }^{* 4}}=1.5 \mathrm{~A}, \mathrm{~V}_{R}^{{ }^{{ }^{5}}}=30 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=3.5 \times 1.6 \times 0.9 \mathrm{~mm} \end{aligned}$ |
|  | RB051LA-40TR |  | $\begin{aligned} & V_{F}{ }^{{ }^{3}}=0.35 \mathrm{~V} \text { max., } \mathrm{I}_{\mathrm{F}}^{{ }^{* 4}=3.0 \mathrm{~A}, \mathrm{~V}_{R}{ }^{{ }^{* 5}}=20 \mathrm{~V},} \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=4.7 \times 2.6 \times 1.05 \mathrm{~mm} \end{aligned}$ |
|  | RB161M-20TR |  | $\begin{aligned} & \mathrm{V}_{F}^{{ }^{3}}=0.31 \mathrm{~V} \text { typ., } \mathrm{I}_{\mathrm{F}}{ }^{{ }^{4}}=1.0 \mathrm{~A}, \mathrm{~V}_{R}^{{ }^{{ }^{5}}}=20 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=3.5 \times 1.6 \times 0.9 \mathrm{~mm} \end{aligned}$ |
|  | RB161SS-20T2R |  | $\begin{aligned} & V_{F}^{{ }^{* 3}}=0.42 \mathrm{~V}, \mathrm{I}_{{ }^{*} 4}=1.0 \mathrm{~A}, \mathrm{~V}_{R}{ }^{{ }^{5}}=20 \mathrm{~V}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=1.6 \times 0.8 \times 0.603 \mathrm{~mm} \end{aligned}$ |
| Capacitor | LMK212BJ106KD | TAIYO YUDEN Co., Ltd. | $\begin{aligned} & 10 \mu \mathrm{~F}, \mathrm{E}_{\mathrm{DC}}{ }^{6}=10 \mathrm{~V}, \mathrm{X} 5 \mathrm{R}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=2.0 \times 1.25 \times 0.95 \mathrm{~mm} \end{aligned}$ |
|  | EMK107B7105KA |  | $\begin{aligned} & 10 \mu \mathrm{~F}, \mathrm{E}_{\mathrm{DC}}{ }^{* 6}=16 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=1.6 \times 0.8 \times 0.9 \mathrm{~mm} \end{aligned}$ |
|  | C1608X5R0J106M | TDK Corporation | $\begin{aligned} & 10 \mu \mathrm{~F}, \mathrm{E}_{\mathrm{Dc}}{ }^{* 6}=6.3 \mathrm{~V}, \mathrm{X} 5 \mathrm{R}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=1.6 \times 0.8 \times 0.9 \mathrm{~mm} \\ & \hline \end{aligned}$ |
|  | C1608X7R1C105K |  | $\begin{aligned} & 1 \mu \mathrm{~F}, \mathrm{E}_{\mathrm{Dc}}{ }^{{ }^{6} 6}=16 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}, \\ & \mathrm{~L} \times \mathrm{W} \times \mathrm{H}=1.6 \times 0.8 \times 0.9 \mathrm{~mm} \end{aligned}$ |

* 1. DCR:

DC resistance
*2. I MAX: Maximum allowable current

* 3. $V_{F}$ : Forward voltage
* 4. $I_{F}$ : Forward current
*5. $\mathrm{V}_{\mathrm{R}}$ : Reverse voltage
* 6. EDC: Rated voltage

Caution The values shown in the characteristics column of Table 16 above are based on the materials provided by each manufacture. However, consider the characteristics of the original materials when using the above products.
2. Output Current (lout) vs. Efficiency ( $\eta$ ) Characteristics, Output Current (lout) vs. Output Voltage (V ${ }_{\text {OUT }}$ ) Characteristics

Following shows the actual output current (lout) vs. efficiency $(\eta)$ and output current (lout) vs. output voltage (Vout) characteristics for conditions 1 to 7 in Table 15.

Condition 1 S-8363B (Vout(s) $=1.8 \mathrm{~V}$ )



Condition 2 S-8363B ( $\mathrm{V}_{\text {out }(\mathrm{s})}=3.3 \mathrm{~V}$ )



Condition 3 S-8363B ( $\mathrm{V}_{\text {out }(\mathrm{S})}=5.0 \mathrm{~V}$ )



Condition 4 S-8363B ( $\mathrm{V}_{\text {out }(\mathrm{S})}=3.3 \mathrm{~V}$ )



Condition 5 S-8363B (Vout(S) $=3.3 \mathrm{~V}$ )



Condition 6 S-8363B ( $\mathrm{VOUT}_{\text {(S })}=3.3 \mathrm{~V}$ )



Condition 7 S-8363B (Vout(s) $=3.3 \mathrm{~V}$ )



## 3. Output Current (IOUT) vs. Ripple Voltage $\left(\mathrm{V}_{\mathrm{r}}\right)$ Characteristics

Following shows the actual output current (lout) vs. ripple voltage $\left(\mathrm{V}_{\mathrm{r}}\right)$ characteristics for conditions of 1 to 7 in Table 15.

Condition 1 S-8363B ( $\mathrm{V}_{\text {out(s) }}=1.8 \mathrm{~V}$ )


Condition 3 S-8363B ( $\mathrm{V}_{\text {out }(\mathrm{S})}=5.0 \mathrm{~V}$ )


Condition 5 S-8363B ( $\mathrm{V}_{\text {OUT(S) }}=3.3 \mathrm{~V}$ )


Condition 7 S-8363B ( $\mathrm{V}_{\mathrm{OUT}(\mathrm{S})}=3.3 \mathrm{~V}$ )


Condition 2 S-8363B ( $\mathrm{V}_{\text {out }(\mathrm{S})}=3.3 \mathrm{~V}$ )


Condition 4 S-8363B ( $\mathrm{V}_{\text {out }(\mathrm{s})}=3.3 \mathrm{~V}$ )


Condition 6 S-8363B ( $\mathrm{V}_{\text {OUT(S) }}=3.3 \mathrm{~V}$ )


## Marking Specification

(1) SNT-6A

(1) to (3) : Product code (Refer to Product name vs. Product code)
(4) to (6) : Lot number

Product name vs. Product code

| Product name | Product code |  |  |
| :--- | :---: | :---: | :---: |
|  | $(1)$ | $(2)$ | $(3)$ |
| S-8363B-I6T1U2 | I | 9 | B |

(2) SOT-23-6


Product name vs. Product code

| Product name | Product code |  |  |
| :--- | :---: | :---: | :---: |
|  | $(1)$ | $(2)$ | $(3)$ |
| S-8363B-M6T1U2 | I | 9 | B |

Remark Please select products of environmental code $=\mathrm{U}$ for $\mathrm{Sn} 100 \%$, halogen-free products.


No. PG006-A-P-SD-2.1

| TITLE | SNT-6A-A-PKG Dimensions |
| :---: | :---: |
| No. | PG006-A-P-SD-2.1 |
| ANGLE | $\ddots$ |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



No. PG006-A-C-SD-2.0

| TITLE | SNT-6A-A-Carrier Tape |
| :---: | :---: |
| No. | PG006-A-C-SD-2.0 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



No. PG006-A-R-SD-1.0

| TITLE | SNT-6A-A-Reel |  |
| :---: | :---: | :---: |
| No. | PG006-A-R-SD-1.0 |  |
| ANGLE |  | QTY. |
|  | 5,000 |  |
| UNIT | mm |  |
|  |  |  |
| ABLIC Inc. |  |  |


0.20 .3 ※ 1
※1．ランドパターンの幅に注意してください（ 0.25 mm min．／ 0.30 mm typ．）。
※2．パッケージ中央にランドパターンを広げないでください $(1.30 \mathrm{~mm} \sim 1.40 \mathrm{~mm})$ 。
注意 1．パッケージのモールド樹脂下にシルク印刷やハンダ印刷などしないでください。
2．パッケージ下の配線上のソルダーレジストなどの厚みをランドパターン表面から 0.03 mm以下にしてください。
3．マスク開ロサイズと開ロ位置はランドパターンと合わせてください。
4．詳細は＂SNTパッケージ活用の手引き＂を参照してください。
※1．Pay attention to the land pattern width（ 0.25 mm min．／ 0.30 mm typ．）．
※2．Do not widen the land pattern to the center of the package（ $1.30 \mathrm{~mm} \sim 1.40 \mathrm{~mm}$ ）．
Caution 1．Do not do silkscreen printing and solder printing under the mold resin of the package．
2．The thickness of the solder resist on the wire pattern under the package should be 0.03 mm or less from the land pattern surface．
3．Match the mask aperture size and aperture position with the land pattern．
4．Refer to＂SNT Package User＇s Guide＂for details．
※1．请注意焊盘模式的宽度（ 0.25 mm min．／ 0.30 mm typ．）。
※2．请勿向封装中间扩展焊盘模式（ $1.30 \mathrm{~mm} \sim 1.40 \mathrm{~mm}$ ）。
注意 1．请勿在树脂型封装的下面印刷丝网，焊锡。
2．在封装下，布线上的阻焊膜厚度（从焊盘模式表面起）请控制在 0.03 mm 以下。
3．钢网的开口尺寸和开口位置请与焊盘模式对齐。
4．详细内容请参阅＂SNT 封装的应用指南＂。

No．PG006－A－L－SD－4． 1

| TITLE | SNT－6A－A <br> －Land Recommendation |
| :---: | :---: |
| No． | PG006－A－L－SD－4．1 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc． |  |



| TITLE | SOT236-A-PKG Dimensions |
| :---: | :---: |
| No. | MP006-A-P-SD-2.1 |
| ANGLE | $\square$ |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



No. MP006-A-C-SD-3. 1

| TITLE | SOT236-A-Carrier Tape |
| :---: | :---: |
| No. | MP006-A-C-SD-3.1 |
| ANGLE |  |
| UNIT | mm |
|  |  |
|  |  |
| ABLIC Inc. |  |



No. MP006-A-R-SD-2. 1

| TITLE | SOT236-A-Reel |  |  |
| :---: | :---: | :---: | :---: |
|  | MP006-A-R-SD-2.1 |  |  |
| ANGLE |  | QTY |  |
|  | 3,000 |  |  |
| UNIT | mm |  |  |
|  |  |  |  |
| ABLIC Inc. |  |  |  |

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