[LDO Regulator](https://www.onsemi.com/products/power-management/dc-dc-controllers-converters-regulators/ldo-regulators-linear-voltage-regulators) - Watchdog, **RESET**

5.0 V, 3.3 V, 250 mA

The NCV8508B is a precision micropower Low Dropout (LDO) voltage regulator. The part contains many of the required features for powering microprocessors. Its robustness makes it suitable for severe automotive environments. In addition, the NCV8508B is ideal for use in battery operated, microprocessor controlled equipment because of its extremely low quiescent current.

Features

- Output Voltage: 5.0 V and 3.3 V
- ±3.0% Output Voltage
- I_{OUT} Up to 250 mA
- Quiescent Current Independent of Load
- Micropower Compatible Control Functions:
	- ♦ Wakeup
	- ♦ Watchdog
	- ♦ RESET
- Low Quiescent Current (100 µA typ)
- Protection Features:
- Thermal Shutdown
	- Short Circuit
	- ♦ 45 V Operation
- NCV Prefix for Automotive and Other Applications Requiring Site and Change Controls
- AEC Qualified
- PPAP Capable
- These are Pb−Free Devices

*C1 required if regulator is located far from power supply filter.

Figure 1. Application Circuit

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MARKING DIAGRAMS

V8508yBxx

O

ORDERING INFORMATION

See detailed ordering and shipping information in the package dimensions section on page [20](#page-19-0) of this data sheet.

PIN CONNECTIONS

PACKAGE PIN DESCRIPTION

Figure 2. Block Diagram

MAXIMUM RATINGS

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

1. 60 second maximum above 183°C.

2. −5°C/+0°C allowable conditions.

THERMAL CHARACTERISTICS

See Package Thermal Data Section (Page [11](#page-10-0))

ELECTRICAL CHARACTERISTICS (–40°C ≤ Tյ ≤ 125°C; 6.0 V ≤ V_{IN} ≤ 28 V, 100 μA ≤ I_{OUT} ≤ 150 mA, C₂ = 1.0 μF, R_{Delay} = 60 k; unless otherwise specified.)

RESET

WATCHDOG INPUT

WAKEUP OUTPUT (V_{IN} = 14 V, I_{OUT} = 5.0 mA)

[3](#page-4-0). Measured when the output voltage has dropped 100 mV from the nominal value. (see Figure [12](#page-7-0))

[4](#page-4-0). Current drain on the Delay pin directly affects the Delay Time, Wakeup Period, and the RESET to Wakeup Delay Time.

ELECTRICAL CHARACTERISTICS (–40°C ≤ Tյ ≤ 125°C; 6.0 V ≤ V_{IN} ≤ 28 V, 100 μA ≤ I_{OUT} ≤ 150 mA, C₂ = 1.0 μF, R_{Delay} = 60 k; unless otherwise specified.)

3. Measured when the output voltage has dropped 100 mV from the nominal value. (see Figure [12](#page-7-0))

4. Current drain on the Delay pin directly affects the Delay Time, Wakeup Period, and the RESET to Wakeup Delay Time.

TIMING DIAGRAMS

Figure 3. Power Up, Sleep Mode and Normal Operation

Figure 5. Power Down and Restart Sequence

TYPICAL PERFORMANCE CHARACTERISTICS

TYPICAL PERFORMANCE CHARACTERISTICS

DEFINITION OF TERMS

Dropout Voltage: The input−output voltage differential at which the circuit ceases to regulate against further reduction in input voltage. Measured when the output voltage has dropped 100 mV from the nominal value obtained at 14 V input, dropout voltage is dependent upon load current and junction temperature.

Input Voltage: The DC voltage applied to the input terminals with respect to ground.

Line Regulation: The change in output voltage for a change in the input voltage. The measurement is made under conditions of low dissipation or by using pulse techniques

DETAILED OPERATING DESCRIPTION

The NCV8508B is a precision micropower voltage regulator with very low quiescent current (100 µA typical at 250 mA load). A typical dropout voltage is 450 mV at 150 mA for 5 V option. Microprocessor control logic includes Watchdog, Wakeup and RESET. This unique combination of extremely low quiescent current and full microprocessor control makes the NCV8508B ideal for use in battery operated, microprocessor controlled equipment in addition to being a good fit in the automotive environment.

The NCV8508B Wakeup function brings the microprocessor out of Sleep mode. The microprocessor in turn signals its Wakeup status back to the NCV8508B by issuing a Watchdog signal.

The Watchdog logic function monitors an input signal (WDI) from the microprocessor. The NCV8508B responds to the falling edge of the Watchdog signal which it expects at least once during each Wakeup period. When the correct Watchdog signal is received, a falling edge is issued on the Wakeup signal line.

such that the average chip temperature is not significantly affected.

Load Regulation: The change in output voltage for a change in load current at constant chip temperature.

Quiescent Current: The part of the positive input current that does not contribute to the positive load current. The regulator ground lead current.

Ripple Rejection: The ratio of the peak−to−peak input ripple voltage to the peak−to−peak output ripple voltage.

Current Limit: Peak current that can be delivered to the output.

 $\overline{\text{RESET}}$ is independent of V_{IN} and operates correctly to an output voltage as low as 1.0 V. A signal is issued in any of three situations. During power up, the RESET is held low until the output voltage is in regulation. During operation, if the output voltage shifts below the regulation limits, the RESET toggles low and remains low until proper output voltage regulation is restored. Finally, a $\overline{\text{RESET}}$ signal is issued if the regulator does not receive a Watchdog signal within the Wakeup period.

The RESET pulse width, Wakeup signal frequency, and Wakeup delay time are all set by one external resistor, R_{Delay}.

The Delay pin is a buffered bandgap voltage (1.25 V). It can be used as a reference for an external tracking regulator as shown in Figure 17.

The regulator is protected against short circuit and thermal runaway conditions. The device runs through 45 volt transients, making it suitable for use in automotive environments.

Figure 17. Application Circuit

CIRCUIT DESCRIPTION

Functional Description

To reduce the drain on the battery, a system can go into a low current consumption mode whenever it is not performing a main routine. The Wakeup signal is generated continuously and is used to interrupt a microcontroller that is in sleep mode. The nominal output is a 5.0 (or 3.3 V) volt square wave (voltage generated from V_{OUT}) with a duty cycle of 50% at a frequency that is determined by a timing resistor, R_{Delay}.

When the microprocessor receives a rising edge from the Wakeup output, it must issue a Watchdog pulse and check its inputs to decide if it should resume normal operations or remain in the sleep mode.

The first falling edge of the Watchdog signal causes the Wakeup to go low within 2.0 μ s (typ) and remain low until the next Wakeup cycle (see Figure 18). Other Watchdog pulses received within the same cycle are ignored (Figure [3](#page-5-0)).

During power up, RESET is held low until the output voltage is in regulation. During operation, if the output voltage shifts below the regulation limits, the $\overline{\text{RESET}}$ toggles low and remains low until proper output voltage regulation is restored. After the RESET delay, RESET returns high.

The Watchdog circuitry continuously monitors the input Watchdog signal (WDI) from the microprocessor. The absence of a falling edge on the Watchdog input during one Wakeup cycle will cause a **RESET** pulse to occur at the end of the Wakeup cycle. (see Figure [4](#page-5-0)).

The Wakeup output is pulled low during a $\overline{\text{RESET}}$ regardless of the cause of the RESET. After the RESET returns high, the Wakeup cycle begins again (see Figure [4](#page-5-0)).

The RESET Delay Time, Wakeup signal frequency and RESET high to Wakeup delay time are all set by one external resistor R_{Delay}.

Wakeup Period = (4.17×10^{-7}) R_{Delav}

RESET Delay Time = (5.21×10^{-8}) R_{Delay}

RESET HIGH to Wakeup Delay Time = (2.08×10^{-7}) R_{Delay}

Resistor temperature coefficient and tolerance as well as the tolerance of the NCV8508B must be taken into account in order to get the correct system tolerance for each parameter.

Figure 18. Wakeup Response to WDI

Figure 19. Wakeup Response to RESET (Low Voltage)

Recommend Thermal Data for D2PAK−7 Package

5. 1 oz. copper, 118 mm² copper area, 0.062" thick FR4.

6. 1 oz. copper, 626 mm² copper area, 0.062" thick FR4.

Figure 20. PCB Layout and Package Construction for Simulation

Table 1. D2PAK 7−Lead Thermal RC Network Models

NOTE: Bold face items in the Cauer network above, represent the package without the external thermal system. The Bold face items in the Foster network are computed by the square root of time constant R(t) = 166 * sqrt(time(sec)). The constant is derived based on the active area of the device with silicon and epoxy at the interface of the heat generation.

The Cauer networks generally have physical significance and may be divided between nodes to separate thermal behavior due to one portion of the network from another. The Foster networks, though when sorted by time constant (as above) bear a rough correlation with the Cauer networks, are really only convenient mathematical models. Cauer networks can be easily implemented using circuit simulating tools, whereas Foster networks may be more easily implemented using mathematical tools (for instance, in a spreadsheet program), according to the following formula:

$$
R(t)\,=\,\sum_{i\,=\,1}^nR_i\left(1\!-\!e^{-t/tau_i}u_i\,\right)
$$

-JA vs Copper Spreader Area

Figure 22. D2PAK 7−Lead Single Pulse Heating Curve

Figure 24. Grounded Capacitor Thermal Network ("Cauer" Ladder)

Figure 25. Non−Grounded Capacitor Thermal Ladder ("Foster" Ladder)

Recommend Thermal Data for SOIC−8 EP Package

7. 1 oz. copper, 54 mm² copper area, 0.062" thick FR4.

8. 1 oz. copper, 717 mm² copper area, 0.062" thick FR4.

Figure 26. Internal Construction of the Package and PCB Layout for Multiple Pad Area

Table 2. SOIC 8−Lead EP Thermal RC Network Models

NOTE: Bold face items in the Cauer network above, represent the package without the external thermal system. The Bold face items in the Foster network are computed by the square root of time constant R(t) = 225 * sqrt(time(sec)). The constant is derived based on the active area of the device with silicon and epoxy at the interface of the heat generation.

The Cauer networks generally have physical significance and may be divided between nodes to separate thermal behavior due to one portion of the network from another. The Foster networks, though when sorted by time constant (as above) bear a rough correlation with the Cauer networks, are really only convenient mathematical models. Cauer networks can be easily implemented using circuit simulating tools, whereas Foster networks may be more easily implemented using mathematical tools (for instance, in a spreadsheet program), according to the following formula:

$$
R(t)\,=\,\sum_{i\,=\,1}^nR_i\left(1\!-\!e^{-t/tau_i}u_i\,\right)
$$

-JA vs Copper Spreader Area

Figure 30. Grounded Capacitor Thermal Network ("Cauer" Ladder)

Figure 31. Non−Grounded Capacitor Thermal Ladder ("Foster" Ladder)

APPLICATION NOTES

Calculating Power Dissipation in a Single Output Linear Regulator

The maximum power dissipation for a single output regulator (Figure 32) is:

$$
PD(max) = [VIN(max) - VOUT(min)]IOUT(max)
$$

+
$$
VIN(max)IQ
$$
 (1)

where:

 $V_{IN(max)}$ is the maximum input voltage,

 $V_{\text{OUT}(min)}$ is the minimum output voltage,

 $I_{OUT(max)}$ is the maximum output current for the application, and

 I_O is the quiescent current the regulator consumes at $I_{\text{OUT(max)}}$.

Once the value of $P_{D(max)}$ is known, the maximum permissible value of R_{HJA} can be calculated:
 $R_{\text{HIA}} = \frac{150^{\circ} \text{C} - \text{T}_{\text{A}}}{150^{\circ} \text{C} - \text{T}_{\text{A}}}$

$$
R_{\theta J A} = \frac{150^{\circ} C - T_A}{P_D}
$$
 (2)

The value of R_{0JA} can then be compared with those in the package section of the data sheet. Those packages with R_{0JAS} less than the calculated value in Equation 2 will keep the die temperature below 150°C.

In some cases, none of the packages will be sufficient to dissipate the heat generated by the IC, and an external heatsink will be required.

Heatsinks

A heatsink effectively increases the surface area of the package to improve the flow of heat away from the IC and into the surrounding air.

Each material in the heat flow path between the IC and the outside environment will have a thermal resistance. Like series electrical resistances, these resistances are summed to determine the value of $R_{\theta JA}$:

$$
R_{\theta J} = R_{\theta J} C + R_{\theta C} S + R_{\theta S} A \tag{3}
$$

where:

 $R_{\theta JC}$ = the junction–to–case thermal resistance,

 R_{HCS} = the case–to–heatsink thermal resistance, and

 R_{BSA} = the heatsink–to–ambient thermal resistance.

 R_{0JC} appears in the package section of the data sheet. Like $R_{\theta JA}$, it too is a function of package type. $R_{\theta CS}$ and $R_{\theta SA}$ are functions of the package type, heatsink and the interface between them. These values appear in data sheets of heatsink manufacturers.

ORDERING INFORMATION

NOTE: Contact factory for other options.

†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.

PACKAGE DIMENSIONS

PACKAGE DIMENSIONS

*For additional information on our Pb−Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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