LTC2965

100V Micropower Single Voltage Monitor

FEATURES

- **Wide Operating Range: 3.5V to 100V**
- **Wide Monitoring Range: 3.5V to 98V**
- **Quiescent Current: 7µA**
- **Adjustable Threshold Range**
- **Internal High Value Resistive Dividers**
- ±1.4% (Max) Threshold Accuracy Over Temperature
- Polarity Selection
- 100V Rated Outputs
- Selectable Built-In Hysteresis
- 16-Lead MS and 8-Lead 3mm × 3mm DFN Packages

APPLICATIONS
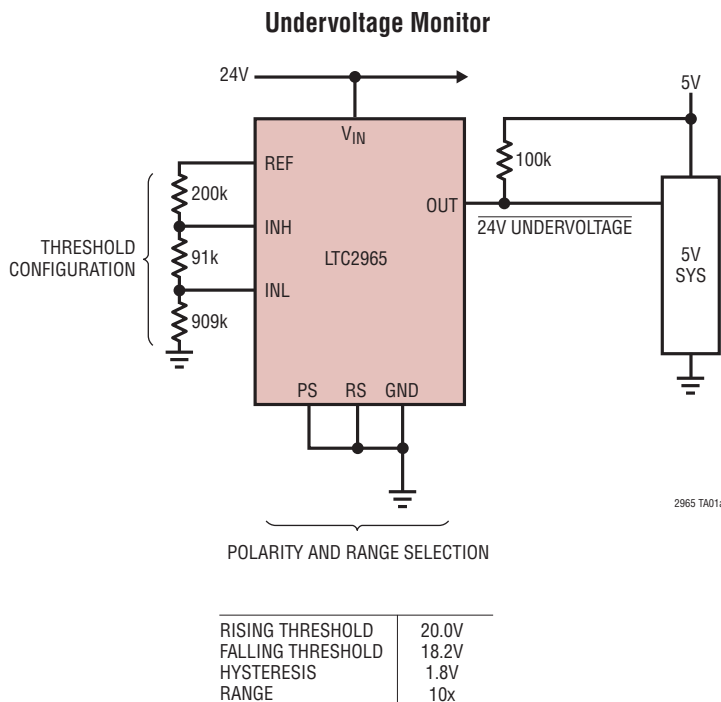
- Portable Equipment
- Battery-Powered Equipment
- Telecom Systems
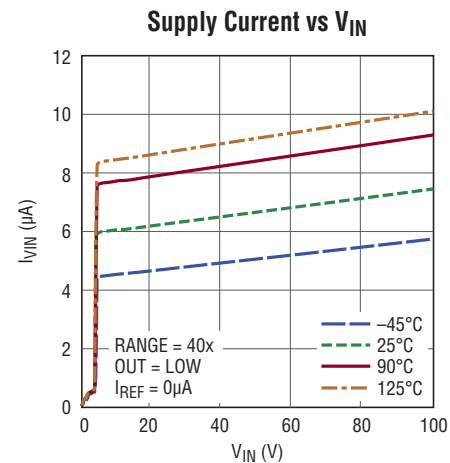- Automotive/Industrial Electronics

DESCRIPTION

The LTC®2965 is a low current, high voltage single channel voltage monitor. Internal high value resistors sense the input monitor pin providing a compact and low power solution for voltage monitoring. Two comparator reference inputs (INH and INL) are included to allow configuration of a high and low threshold using an external resistive divider biased from the on-chip reference. A range selection pin is provided to set the internal resistive divider for 10x or 40x scaling. The thresholds are scaled according to the range selection settings. Additionally, either INH or INL can be grounded to enable built-in hysteresis. Polarity selection pin allows the output to be inverted. The output is 100V capable and includes a 500k pull-up resistor to an internal supply.

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TYPICAL APPLICATION

Undervoltage Monitor

2965 TA01a

RISING THRESHOLD	20.0V
FALLING THRESHOLD	18.2V
HYSTERESIS	1.8V
RANGE	10x

V$_{IN}$ MONITOR RANGE	RANGE SELECTION
3.5V to 24.5V	10x
14V to 98V	40x

Supply Current vs V$_{IN}$

2965 TA01b

ABSOLUTE MAXIMUM RATINGS (Notes 1, 2)

Input Voltages

V_{IN} .... −0.3V to 140V
PS, RS .... −0.3V to 6V
INH, INL.. −0.3V to 6V

Output Voltages

OUT .... −0.3V to 140V

Average Currents

V_{IN} ....−20mA
OUT ....±5mA
REF ....±5mA
INH, INL..−1mA

Operating Ambient Temperature Range

LTC2965C...0°C to 70°C
LTC2965I...−40°C to 85°C
LTC2965H.......................................−40°C to 125°C
Storage Temperature Range ....−65°C to 150°C
Lead Temperature (Soldering, 10 sec)..................300°C

PIN CONFIGURATION

TOP VIEW

V_{IN} 1
REF 2
INH 3
INL 4

9 GND

8 OUT
7 GND
6 RS
5 PS

DD PACKAGE
8-LEAD (3mm × 3mm) PLASTIC DFN
T_{JMAX} = 150°C, θ_{JA} = 43°C/W
EXPOSED PAD (PIN 9) PCB GND CONNECTION OPTIONAL

TOP VIEW

V_{IN} 1
NC 2
NC 3
NC 4
NC 5
REF 6
INH 7
INL 8

16 OUT
15 NC
14 NC
13 NC
12 NC
11 GND
10 RS
9 PS

MS PACKAGE
16-LEAD PLASTIC MSOP
T_{JMAX} = 150°C, θ_{JA} = 120°C/W

ORDER INFORMATION (http://www.linear.com/product/LTC2965#orderinfo)
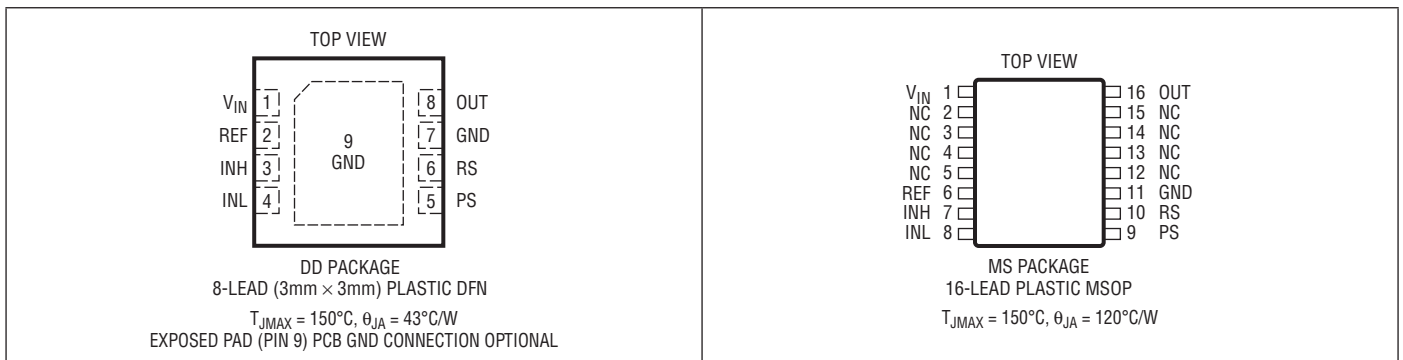
Lead Free Finish

TUBE	TAPE AND REEL	PART MARKING*	PACKAGE DESCRIPTION	TEMPERATURE RANGE
LTC2965CDD#PBF	LTC2965CDD#TRPBF	LGMK	8-Lead (3mm × 3mm) Plastic DFN	0°C to 70°C
LTC2965IDD#PBF	LTC2965IDD#TRPBF	LGMK	8-Lead (3mm × 3mm) Plastic DFN	−40°C to 85°C
LTC2965HDD#PBF	LTC2965HDD#TRPBF	LGMK	8-Lead (3mm × 3mm) Plastic DFN	−40°C to 125°C
LTC2965CMS#PBF	LTC2965CMS#TRPBF	2965	16-Lead Plastic MSOP	0°C to 70°C
LTC2965IMS#PBF	LTC2965IMS#TRPBF	2965	16-Lead Plastic MSOP	−40°C to 85°C
LTC2965HMS#PBF	LTC2965HMS#TRPBF	2965	16-Lead Plastic MSOP	−40°C to 125°C

Consult LTC Marketing for parts specified with wider operating temperature ranges. *The temperature grade is identified by a label on the shipping container.
Consult LTC Marketing for information on nonstandard lead based finish parts.

For more information on lead free part marking, go to: http://www.linear.com/leadfree/
For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/. Some packages are available in 500 unit reels through designated sales channels with #TRMPBF suffix.

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at T_A = 25°C. V_{IN} = 12V, RS = GND, PS = GND, INH = 1.2V, INL = GND (Notes 1, 2).

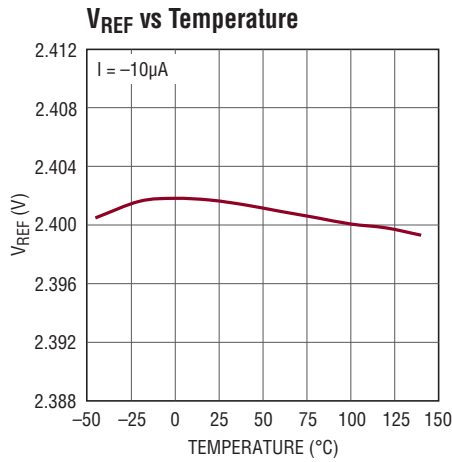| SYMBOL	PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
V_{IN}	Input Supply Operating Range	V_{IN}	●	3.5		100	V
V_{MON}	V_{IN} Monitor Range			3.5		98	V
I_{VIN}	V_{IN} Input Supply Current	V_{IN} = 100V, 40x	●	3	7	15	µA
V_{UVLO}	Undervoltage Lockout	V_{IN} Rising	●			3	V
	Undervoltage Lockout Hysteresis	V_{IN} Falling			70		mV
Comparator Reference Input: INH, INL							
V_{CM}	Comparator Common Mode Voltage		●	0.35		2.45	V
V_{ERR}	V_{IN} Error Voltage at 96V	INH = V_{REF}, 40x 0.35V ≤ INH ≤ 2.4V, 40x	● ●		±250 ±250	±1360 ±400	mV mV
	V_{IN} Error Voltage at 24V	INH = V_{REF}, 10x 0.35V ≤ INH ≤ 2.4V, 10x	● ●		±35 ±35	±315 ±75	mV mV
V_{OS}	Comparator Offset Voltage	INH = 0.35V, 10x	●		±1.9	±3	mV
AV_{ERR}	Internal Resistive Divider Range Error	INH = 2.4V, Range = 10x, 40x	●			±0.4	%
V_{HYS}	Comparator Built-in Hysteresis	INH = GND, INL Rising, V_{IN} = 24V INL = GND , INH Falling, V_{IN} = 24V	● ●	14 −30	22 −22	30 −14	mV mV
V_{HYTH}	Built-in Hysteresis Enable Threshold		●	100		175	mV
t_{PD}	V_{IN} to OUT Comparator Propagation Delay	Overdrive = 10%, OUT Falling,10x INH = GND, INL = 1.2V	●		40	80	µs
$I_{IN(LKG)}$	Input Leakage Current (INH, INL)	V = 1.2V, I-Grade V = 1.2V, H-Grade	● ●		±0.1 ±0.1	±1 ±10	nA nA
Reference: REF							
V_{REF}	Reference Output Voltage	I_{REF} ≤ 100µA, V_{IN} ≥ 3.5V	●	2.378	2.402	2.426	V
Noise	Reference Output Noise	100Hz to 100kHz			140		µV$_{RMS}$
Control Inputs: RS, PS							
V_{TH}	Select Input Threshold		●	0.4		1.4	V
I_{LKG}	Input Leakage Current	V = 2.4V	●			±100	nA
Status Outputs: OUT							
V_{OL}	Voltage Output Low	V_{IN} = 1.25V, I = 10µA V_{IN} = 3.5V, I = 500µA	● ●			100 400	mV mV
V_{OH}	Voltage Output High	V_{IN} = 3.5V, I = −1µA V_{IN} ≥ 4.5V, I = −1µA	● ●	2 2.8	2.375 3	2.75 4	V V
I_{OH}	Output Current High	V = GND, V_{IN} = 3.5V	●	−15	−7.5	−5	µA
$I_{O(LKG)}$	Leakage Current, Output High	V = 100V, V_{IN} = 6V	●			±250	nA

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

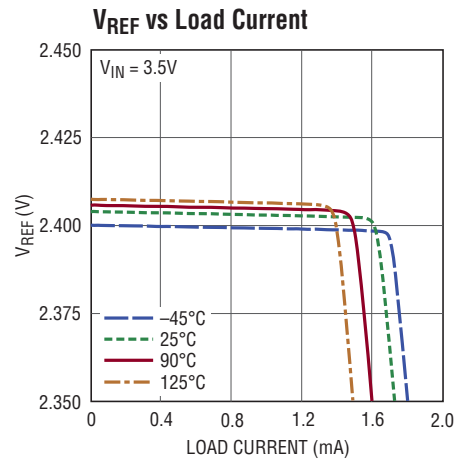**Note 2:** All currents into pins are positive; all voltages are referenced to GND unless otherwise noted.
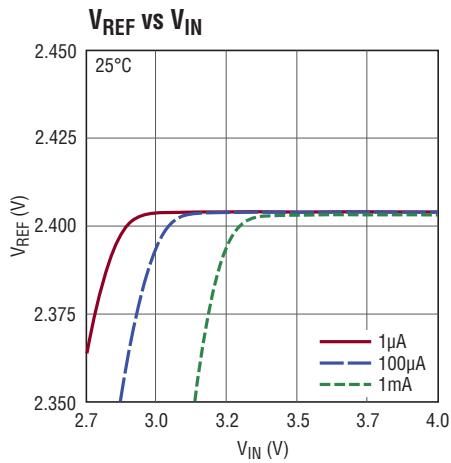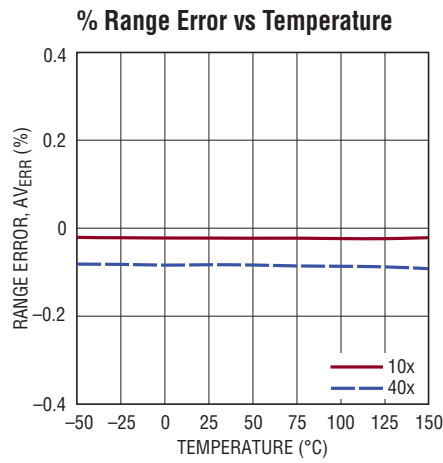
TYPICAL PERFORMANCE CHARACTERISTICS

Supply Current vs V$_{IN}$

RANGE = 40x
OUT = LOW
I$_{REF}$ = 0µA

−45°C
25°C
90°C
125°C

2965 G01

V$_{REF}$ vs Temperature

I = −10µA

2965 G02

V$_{REF}$ vs Load Current

V$_{IN}$ = 3.5V

−45°C
25°C
90°C
125°C

2965 G03

V$_{REF}$ vs V$_{IN}$

25°C

1µA
100µA
1mA

2965 G04

% Range Error vs Temperature

10x
40x

2965 G05

Comparator V$_{OS}$ vs Temperature

V$_{INH(L)}$ = 1.2V

2965 G06

V$_{IN}$ Falling Propagation Delay vs % Overdrive

V$_{INL}$ = 1.2V
V$_{INH}$ = GND
V$_{IN}$ = 12V

−45°C
25°C
90°C
125°C

2965 G10

Built-In Hysteresis vs Temperature

V$_{INH(L)}$ = 1.2V

2965 G08

2965fc

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TYPICAL PERFORMANCE CHARACTERISTICS

Voltage Output High vs Pull-Down Current (OUT)

$V_{IN} = 12V$

-45°C
25°C
90°C
125°C

V_{OH} (V)

PULL-DOWN CURRENT (µA)

2965 G09

Voltage Output Low vs Pull-Up Current (OUT)

-45°C
25°C
90°C
125°C

V_{OL} (V)

PULL-UP CURRENT (mA)

2965 G10

Voltage Output High vs Input Voltage

$I = -1µA$

V_{OH} (V)

V_{IN} (V)

2965 G11

PIN FUNCTIONS

Exposed Pad (DD8 Only): Exposed pad may be left floating or connected to device ground.

GND: Device Ground.

INH: High Comparator Reference Input. Voltage on this pin is multiplied by the configured range setting to set the V_{IN} high or rising threshold. Keep within valid voltage range, V_{CM}, or tie to GND to configure built-in hysteresis where high threshold for V_{IN} becomes INL + V_{HYS} scaled according to the RS pin configuration.

INL: Low Comparator Reference Input. Voltage on this pin is multiplied by the configured range setting to set the V_{IN} low or falling threshold. Keep within valid voltage range, V_{CM}, or tie to GND to configure built-in hysteresis where low threshold becomes INH – V_{HYS} scaled according to the RS pin configuration. Otherwise, INH-INL sets the hysteresis of the comparator. Oscillation will occur if INL > INH unless built-in hysteresis is enabled.

OUT: Comparator Output. OUT consists of a high voltage active pull-down and a gated, resistive (500kΩ) pull-up

to an internally generated supply between 3.5V and 5V depending on input supply voltage. Blocking circuitry at the pin allows the pin to be resistively pulled up to voltages as high as 100V without back conducting onto the internal supply of the part. Polarity with respect to the V_{IN} pin is configured using the polarity select pin, PS. OUT pulls low when the part is in UVLO.

PS: Polarity Selection. Connect to REF or a voltage >V_{TH} to configure comparator output to be inverting with respect to V_{IN}. Otherwise connect pin to GND to configure comparator output to be noninverting with respect to V_{IN}.

REF: Reference Output. V_{REF} with respect to GND. Use a maximum of 1nF to bypass unless damping resistor is used.

RS: Range Select Input. RS selects 10x or 40x range. Connect to REF or GND to configure pin. (See Table 1)

V_{IN}: Voltage Monitor and Supply Input. An internal high value resistive divider is connected to the pin. If V_{IN} falls below the UVLO threshold minus hysteresis, the output is pulled low. If V_{IN} < 1.2V, the logic state of the outputs cannot be guaranteed.

BLOCK DIAGRAMS
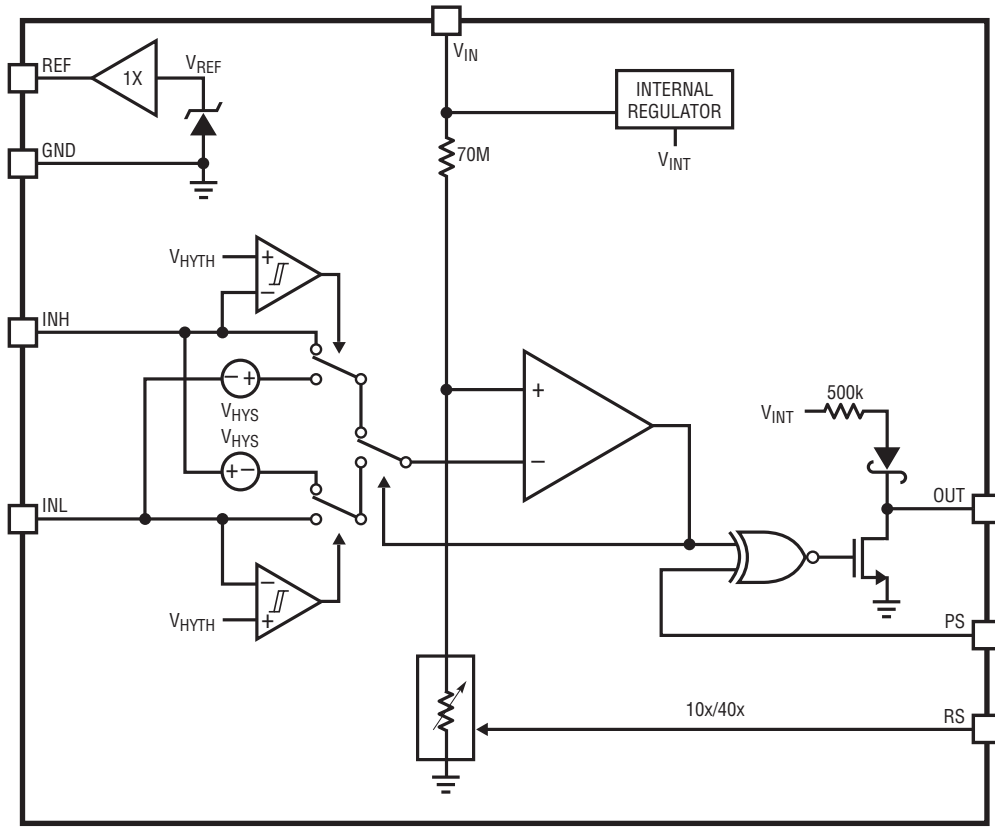
2965 BD

OPERATION

The LTC2965 is a micropower single channel voltage monitor with a 100V maximum operating voltage. Its channel is comprised of an internal high value resistive divider and a comparator with a high voltage output. A reference voltage is provided to allow the thresholds to be set independently. This configuration has the advantage of being able to monitor very high voltages with very little current draw while threshold programming is done using low value resistors at low voltages. Integration of a resistive divider for high voltage sensing makes the LTC2965 a compact and low power solution for generating voltage status signals to a monitoring system.

A built-in buffered reference gives the monitor flexibility to operate independently from a high voltage supply without the requirement of additional low voltage biasing. The reference provides an accurate voltage from which a resistive divider to ground configures the threshold voltage for the internal comparator. In addition, the REF pin can be used as a logic high voltage for the range and polarity select pins.

The input voltage threshold at V_{IN} is determined by the voltage on the INH and INL pins which are scaled by the internal resistive divider. The LTC2965 offers two range settings to select from, 10x and 40x, using the RS pin. Use Table 1 to determine the correct configuration for a desired range setting. The polarity select pin, (PS), configures the OUT pin to be inverting or noninverting with respect to V_{IN} allowing the part to be configured for monitoring overvoltage and undervoltage conditions with either polarity output.

Table 1.

| V_{IN} MONITOR RANGE	RANGE SELECTION	RS
3.5V to 24.5V	10x	L
14V to 98V	40x	H

The INH pin determines the high or rising edge threshold for V_{IN}. If the monitored voltage connected to V_{IN} rises to the scaled INH voltage then the OUT pin is pulled high assuming PS is ground. Likewise, the INL pin determines the low or falling edge threshold for V_{IN} in each channel. If V_{IN} falls to the scaled INL voltage then the OUT pin is

pulled low assuming PS is ground. The amount of hysteresis referred to V_{IN} is the difference in voltage between INH and INL scaled according to the RS pin configuration. INH and INL have an allowable voltage range, V_{CM}. Figure 1 shows the allowable monitor voltage at V_{IN} for each range as a function of comparator reference input voltage (INL/INH).

Typically, an external resistive divider biased from REF is used to generate the INH and INL pin voltages. A built-in hysteresis feature requiring only two resistors can be enabled on either the V_{IN} rising edge by grounding INH or on the falling edge by grounding INL. For example, it is appropriate to ground INH to activate rising edge hysteresis if an accurate falling voltage threshold is required for undervoltage detection. Conversely, it is appropriate to ground INL for falling edge built-in hysteresis if an accurate overvoltage threshold is required. Do not ground both INH and INL. Oscillation occurs if $V_{INL} > V_{INH}$ unless INH built-in hysteresis is enabled.

The high voltage OUT pins have the capability to be pulled up to a user defined voltage as high as 100V with an external resistor. The LTC2965 also includes an internal 500k pull-up resistor to an internal voltage between 3.5V and 5V depending on input voltage. (See V_{OH} in Electrical Characteristics).

If the V_{IN} pin falls below the UVLO threshold then the OUT pin is pulled low regardless of the PS pin state.
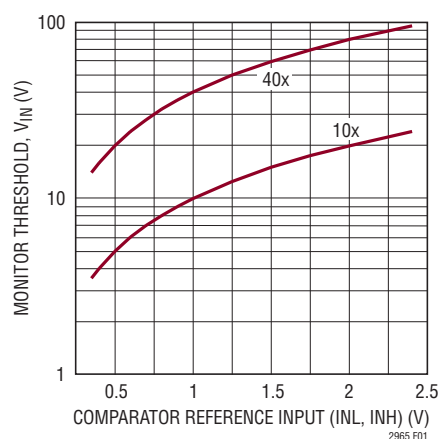
Figure 1. Monitor Threshold
vs Comparator Reference Inputs

APPLICATIONS INFORMATION

Threshold Configuration

The LTC2965 channel monitors the voltage applied to the V_{IN} input. A comparator senses the V_{IN} pin on one of its inputs through the internal resistive divider. The other input is connected to INH/INL that is in turn biased with external resistive dividers off of the REF pin as shown in Figure 2a and 2b. The V_{IN} rising and falling thresholds are determined by:

$$V_{IN(RISE)} = RANGE \cdot V_{INH}$$

$$V_{IN(FALL)} = RANGE \cdot V_{INL}$$

Where RANGE is the configured range of the internal resistive divider. In order to set the threshold for the LTC2965, choose an appropriate range setting for the desired V_{IN} voltage threshold such that the INH and INL voltages are within the specified common mode range, V_{CM}. For example, if a falling threshold of 18V is desired for monitoring a 24V power supply then a range greater than 10x is allowed. However, to maximize the accuracy of the V_{IN} threshold the smallest acceptable range is used, 10x in this case. To implement 2V of hysteresis referred to V_{IN} this means:

$$V_{INH} = 2V, V_{INL} = 1.8V$$

With 10x range the V_{IN} thresholds are:

$$V_{IN(RISE)} = 20V, V_{IN(FALL)} = 18V$$

One possible way to configure the thresholds is by using three resistors to set the voltages on INH and INL. See Figure 2a. The solution for R1, R2 and R3 provides three equations and three unknowns. Maximum resistor size is governed by maximum input leakage current. The maximum input leakage current below 85°C is 1nA. For a maximum error of 1% due to both input currents, the resistive divider current should be at least 100 times the sum of the leakage currents, or 0.2µA.

If in this example, a leakage current error of 0.1% is desired then the total divider resistance is 1.2MΩ which results in a current of 2µA through this network. For $R_{SUM} = 1.2MΩ$

$$R_{SUM} = R1 + R2 + R3$$

$$R1 = \frac{(V_{INL} \cdot R_{SUM})}{V_{REF}} = \frac{(1.8V \cdot 1.2M\Omega)}{2.402V} = 899.5k\Omega$$

The closest 1% value is 909kΩ. R2 can be determined from:

$$R2 = \frac{(V_{INH} \cdot R_{SUM})}{V_{REF}} - R1$$

$$= \frac{(2V \cdot 1.2M\Omega)}{2.402V} - 909k\Omega = 90.2k\Omega$$

The closest 1% value is 90.9kΩ. R3 can be determined from R_{SUM}:

R3 = R_{SUM} − R1 − R2 = 1.2MΩ − 909kΩ − 90.9kΩ = 200.1kΩ

The closest 1% value is 200kΩ. Plugging the standard values back into the equations yields the design values for the V_{INH} and V_{INL} voltages:

$$V_{INH} = 2.002V, V_{INL} = 1.819V$$

The corresponding threshold voltages are:

$$V_{IN(RISE)} = 20.01V, V_{IN(FALL)} = 18.19V$$

Another possible way to configure the thresholds is with independent dividers using two resistors per threshold to set the voltages on INH and INL. See Figure 2b. Care must be taken such that the thresholds are not set too close to each other, otherwise the mismatch of the resistors may cause the voltage at INL to be greater than the voltage at INH which may cause the comparator to oscillate.

As in the previous example, if $R_{SUM} = 1.2MΩ$ is chosen and the target for V_{INL} is 1.8V:

$$R_{SUM} = R1 + R2$$

$$R1 = \frac{(V_{INL} \cdot R_{SUM})}{V_{REF}} = \frac{(1.8V \cdot 1.2M\Omega)}{2.402V} = 899.5k\Omega$$

The closest 1% value is 909kΩ. R2 can be determined by:

$$R2 = (V_{REF} - V_{INL}) \cdot \frac{R1}{V_{INL}}$$

$$= (2.402V - 1.8V) \cdot \frac{(909k\Omega)}{1.8V} = 304k\Omega$$

APPLICATIONS INFORMATION

The closest 1% value is 301kΩ. Plugging the standard values back into the equation for V_{INL} yields the design voltage for V_{INL}:

$$V_{INL} = \frac{(R1 \bullet V_{REF})}{(R1 + R2)} = \frac{(909k\Omega \bullet 2.402V)}{(301k\Omega + 909k\Omega)} = 1.804V$$

At this point in the independent divider example only the values required to set the voltage at INL have been found. Repeat the process for the INH input by substituting the above equations with V_{INH} for V_{INL}, R3 for R1, R4 for R2 and V_{INH} = 2.0V.
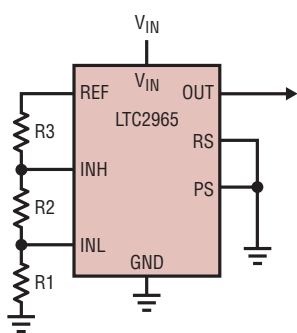
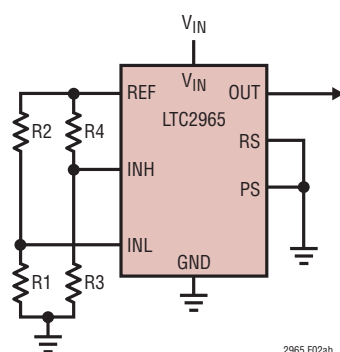**Figure 2a. Three-Resistor Threshold Configuration**

Figure 2b. Two-Resistor Threshold Configuration

Using Built-In Hysteresis

The LTC2965 has the capability of simplifying the threshold configuration such that only two resistors are required. The device pins can be configured to select a built-in hysteresis voltage, V_{HYS}, which can be applied to either the rising or falling threshold depending on whether the INH or INL pin is grounded. Note that the hysteresis voltage at each range setting remains at a fixed value. Figure 3 introduces examples of each configuration. For example, if INH is biased from an external divider and the INL pin is grounded, then hysteresis is enabled on the low or falling threshold. The low threshold is then $-V_{HYS}$ relative to the high threshold determined by INH. Figure 3a introduces built-in hysteresis on the rising edge because INH is pulled to ground. A two-resistor network, R1 and R2, is used to set the voltage on INL using:

$$\frac{R2}{R1} = \frac{V_{REF}}{V_{INL}} - 1$$

Using built-in hysteresis, the V_{INA} thresholds are:

$$V_{IN(RISE)} = RANGE \bullet (INL + V_{HYS})$$

$$V_{IN(FALL)} = RANGE \bullet INL$$

Figure 3b introduces built-in hysteresis on the falling edge because INL is pulled to ground. Similarly, a two-resistor network, R3 and R4, is used to set the voltage on INH using:

$$\frac{R4}{R3} = \frac{V_{REF}}{V_{INH}} - 1$$

Using built-in hysteresis the V_{IN} thresholds are:

$$V_{IN(RISE)} = RANGE \bullet INH$$

$$V_{IN(FALL)} = RANGE \bullet (INH - V_{HYS})$$

Consider V_{INH} = 2V with built-in hysteresis activated on the falling edge. For 10x range, 1.1% falling hysteresis is obtained. If a larger percentage of hysteresis is desired then V_{INH} is alternatively set to 0.5V and the range is selected to be 40x to obtain the same V_{IN} threshold but with 4.4% falling hysteresis. The amount of built-in hysteresis is scaled according to Table 2. If more hysteresis is needed then it is implemented in the external resistive divider as described in the Threshold Configuration section.
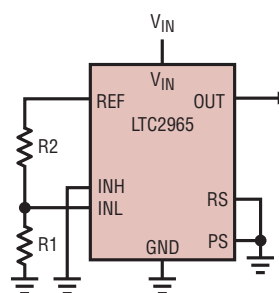

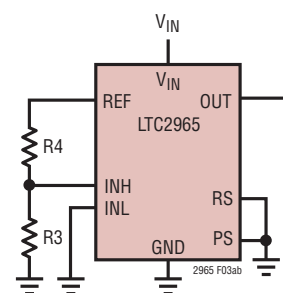**Figure 3a. Rising Edge Built-In Hysteresis**

Figure 3b. Falling Edge Built-In Hysteresis

Table 2. Built-In Hysteresis Voltage vs Range

RANGE	V_{IN} REFERRED BUILT-IN HYSTERESIS
10x	220mV
40x	880mV

APPLICATIONS INFORMATION

Error Analysis

V_{IN} thresholds are subject to the following errors:

- REF Voltage Variation (ΔV_{REF})
- Comparator Offset (V_{OS})
- Internal Divider Range Error (A_{VERR})
- External Resistive Divider Error (A_{XERR})

The effect these errors have on the V_{IN} threshold is expressed by:

$$V_{ERR} = RANGE \bullet \left[\pm V_{OS} \pm \Delta V_{REF} \bullet \frac{V_{INH(L)}}{V_{REF}} \pm V_{INH(L)} \bullet A_{XERR} \right]$$

$$\pm RANGE \bullet A_{VERR} \bullet V_{INH(L)}$$

$$A_{XERR} = 2 \bullet \frac{TOLERANCE}{100} \bullet \left(1 - \frac{V_{INH(L)}}{V_{REF}} \right)$$

External divider error is determined by the percentage tolerance values of the resistors. If 1% tolerance resistors are used in the external divider then there is a 2% worst-case voltage error associated with it. The effects of comparator offset and V_{REF} voltage are uncorrelated with each other. Therefore, a Root-Sum-Square can be applied to the error voltage referred to V_{IN}. Using the example from Threshold Configuration and assuming 1% resistors implement the external resistive divider, the falling V_{IN} threshold of approximately 18V has an error tolerance of:

$$V_{ERR(REF)} = (RANGE)\left(\pm \Delta V_{REF} \bullet \frac{V_{INL}}{V_{REF}} \right)$$

$$= (10) \bullet \left(\pm 24mV \bullet \frac{1.8V}{2.402V} \right) = \pm 180mV$$

$$V_{ERR(EXT)} = (RANGE)\left(\pm V_{INL} \bullet 2 \bullet 0.01 \bullet \left(1 - \frac{V_{INL}}{V_{REF}} \right) \right)$$

$$= (10) \bullet (\pm 1.8V \bullet 0.005) = \pm 90mV$$

$$V_{ERR(VOS)} = (RANGE)(\pm \Delta V_{OS}) = (10) \bullet (\pm 3mV) = \pm 30mV$$

$$V_{ERR(RS)} = (RANGE)(\pm A_{VERR})(\pm V_{INL})$$

$$= (10) \bullet (\pm 0.004) \bullet (1.8V) = \pm 72mV$$

$$V_{ERR} = \sqrt{V^2_{ERR(REF)} + V^2_{ERR(EXT)} + V^2_{ERR(VOS)} + V^2_{ERR(RS)}}$$

$$= \sqrt{(\pm 180mV)^2 + (\pm 90mV)^2 + (\pm 30mV)^2 + (\pm 72mV)^2}$$

$$= \pm 216mV$$

The actual V_{IN} falling threshold has an error tolerance of ±216mV or ±1.2%.

Improving Threshold Accuracy

The biggest threshold error terms are:

- External Resistive Divider Accuracy
- REF Voltage Variation

Even using 1% tolerance resistors, external resistive divider accuracy still accounts for as much as ±2% threshold error while REF voltage variation accounts for ±1% threshold error. In order to minimize these threshold error terms, an external reference can be used to set the thresholds for INH/INL as shown in Figure 4. An LT6656-2.048 has an initial accuracy of 0.05% and provides bias via the 0.1% resistive divider network for INH and INL. It is biased off of the LTC2965 REF pin. The threshold error tolerance is calculated using the method described in the Typical Applications section with $\Delta V_{REF} = \pm 1.024mV$ given the initial accuracy of the LT6656 2.048V output and using 0.1% tolerance resistors for the external divider.

$$V_{ERR(REF)} = (RANGE)\left(\pm \Delta V_{REF} \bullet \frac{V_{INL}}{V_{REF}} \right)$$

$$= (10) \bullet \left(\pm 1.024mV \bullet \frac{1.8V}{2.048V} \right) = \pm 9mV$$

$$V_{ERR(EXT)} = (RANGE)\left(\pm V_{INL} \bullet 2 \bullet 0.001 \bullet \left(1 - \frac{V_{INL}}{V_{REF}} \right) \right)$$

$$= (10) \bullet (\pm 1.8V \bullet 0.0005) = \pm 9mV$$

$$V_{ERR(VOS)} = (RANGE)(\pm \Delta V_{OS}) = (10) \bullet (\pm 3mV) = \pm 30mV$$

$$V_{ERR(RS)} = (RANGE)(\pm A_{VERR})(\pm V_{INL})$$

$$= (10) \bullet (\pm 0.004) \bullet (1.8V) = \pm 72mV$$

$$V_{ERR} = \sqrt{V^2_{ERR(REF)} + V^2_{ERR(EXT)} + V^2_{ERR(VOS)} + V^2_{ERR(RS)}}$$

$$= \sqrt{(\pm 9mV)^2 + (\pm 9mV)^2 + (\pm 30mV)^2 + (\pm 72mV)^2}$$

$$= \pm 79mV$$

The resulting V_{IN} threshold error is reduced to ±0.44% from ±1.2% in the previous error analysis example.
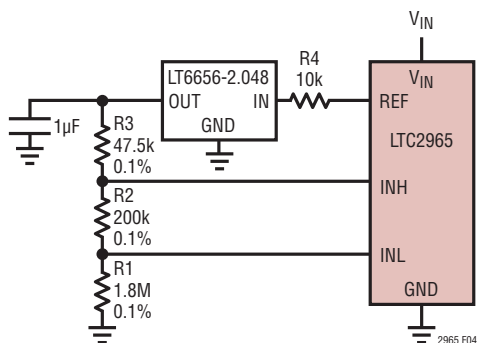
APPLICATIONS INFORMATION

Figure 4. Reducing V$_{IN}$ Threshold Error

Output Configuration with Polarity Selection

The OUT pin may be used with a wide range of user-defined voltages up to 100V with an external resistor. Select a resistor compatible with desired output rise time and load current specifications. When the status outputs are low, power is dissipated in the pull-up resistors. An internal pull-up is present if the OUT pins are left floating or if low power consumption is required. The internal pull-up resistor does not draw current if an external resistor pulls OUT up to a voltage greater than V$_{OH}$.

If PS is connected to ground, the comparator output is noninverting. This means that OUT pulls low when V$_{IN}$ falls below the scaled INL voltages. OUT is released after V$_{IN}$ rises above the scaled INH voltage. Likewise, if PS is connected up to REF or a voltage > V$_{TH}$, the comparator output is inverting. This means that OUT pulls low when V$_{IN}$ rises above the scaled INH voltage and is released when V$_{IN}$ falls below the scaled INL voltage.

If the V$_{IN}$ pin falls below the UVLO threshold minus hysteresis, the output is pulled to ground. The output is guaranteed to stay low for V$_{IN}$ ≥ 1.25V regardless of the output logic configuration.

It is recommended that circuit board traces associated with the OUT pin be located on a different layer than those associated with the INH/INL and REF pins where possible to avoid capacitive coupling.

Hot Swap Events

The LTC2965 can withstand high voltage transients up to 140V. However, when a supply voltage is abruptly

connected to the input resonant ringing can occur as a result of series inductance. The peak voltage could rise to 2x the input supply, but in practice can reach 2.5x if a capacitor with a strong voltage coefficient is present. Circuit board trace inductances of as little as 10nH can produce significant ringing. Ringing beyond the absolute maximum specification can be destructive to the part and should be avoided whenever possible. One effective means to eliminate ringing seen at the V$_{IN}$ pins and to protect the part is to include a 1kΩ to 5kΩ resistance between the monitored voltage and the V$_{IN}$ pin as shown in Figure 5. This provides damping for the resonant circuit. If there is a decoupling capacitor on the V$_{IN}$ pins the time constant formed by the RC network should be considered.
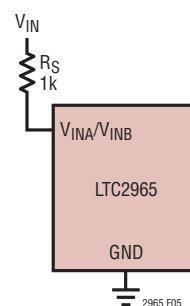

Figure 5. Hot Swap Protection

High Voltage Pin Creepage/Clearance Options

Appropriate spacing between component lead traces is critical to avoid flashover between conductors. There are multiple industry and safety standards that have different spacing requirements depending on factors such as operating voltage, presence of conformal coat, elevation, etc. The LTC2965 is available in a 16-lead MSOP package which offers landing clearance of at least 0.79mm (0.031in). The package incorporates unconnected pins between all adjacent high voltage and low voltage pins to maximize PC board trace clearance. For voltages >30V the MSOP should be used, otherwise the smaller or DFN is sufficient when clearance is not an issue. For more information, refer to the printed circuit board design standards described in IPC2221 and UL60950.

2965fc

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APPLICATIONS INFORMATION

Voltage Reference

The REF pin is a buffered reference with a voltage of V_{REF} referenced to GND. A bypass capacitor up to 1000pF in value can be driven by the REF pin directly. Larger capacitances require a series resistance to dampen the transient response as shown in Figure 6A. If a resistive divider is already present then the bypass capacitor can be connected to the INH or INL pin as shown in Figure 6B. Figure 6C shows the resistor value required for different capacitor values to achieve critical damping. Bypassing the reference can help prevent false tripping of the comparators by preventing glitches on the INH/INL pins. Figure 7 shows the reference load transient response. Figure 8 shows the reference line transient response. If there is a decoupling capacitor on the INH/INL pin the time constant formed by the RC network should be considered. Use a capacitor with a compatible voltage rating.
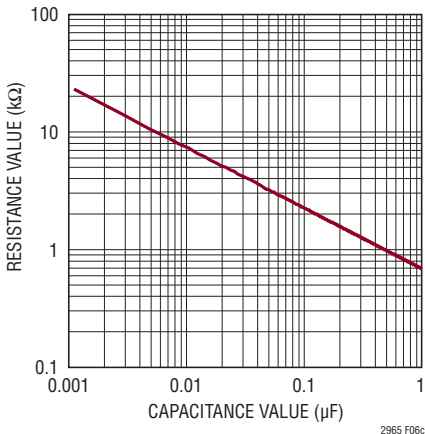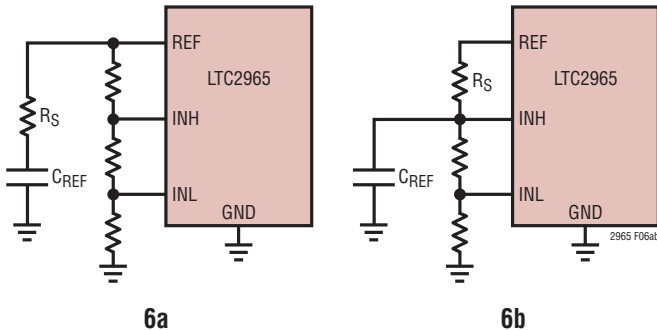
Figure 7. V_{REF} Load Transient

Figure 8. V_{REF} Line Transient

6a

6b

6c

Figure 6. Using Series Resistance to Dampen REF Transient Response
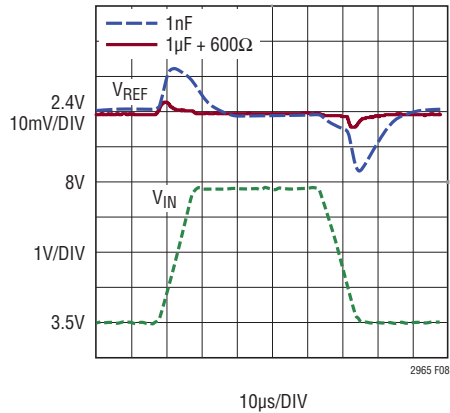
TYPICAL APPLICATIONS

Negative Voltage Monitor with Output Level Shift

Figure 9 illustrates an LTC2965 configured to monitor a –15V supply with a level-shifted output to a 5V supply. Q1 buffers the digital input of the 5V system from the –15V supply and prevents UV from going below GND. The OUT pin drives the base of Q1 through a resistor network comprised of R3 and R4. Keep R4/R3 ≥0.4 to ensure there is proper base current to pull UV to ground. If an exposed pad is present it should be tied to the LTC2965 GND pin or left open.
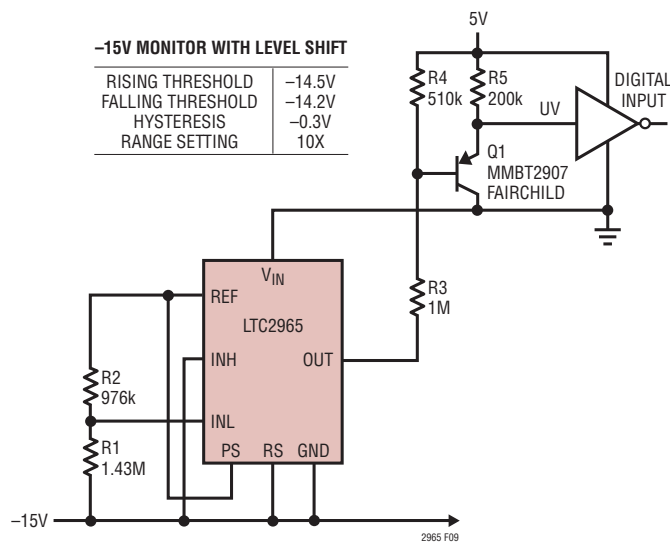
Current Sink/Source

The LTC2965 can be used as a high voltage current source or a current sink as shown in Figure 10. The current is determined by placing a resistive load, R_{SET}, on the REF pin. The total current is then $V_{REF}/R_{SET} + I_{VA}$ because the bias current of the part adds a small error term. Part of the bias current is the internal resistive divider which is approximately 78MΩ with the RS pin configured to 10x.

−15V MONITOR WITH LEVEL SHIFT	
RISING THRESHOLD	−14.5V
FALLING THRESHOLD	−14.2V
HYSTERESIS	−0.3V
RANGE SETTING	10X

Figure 9. Negative Voltage Monitor with Output Level Shift to a 5V Digital Input

Current Sink
$I_{SET} = V_{REF}/R_{SET}$

$I_{ERROR} = (V_{REF}/R_{SET}) − I_{SUPPLY}$

Current Source
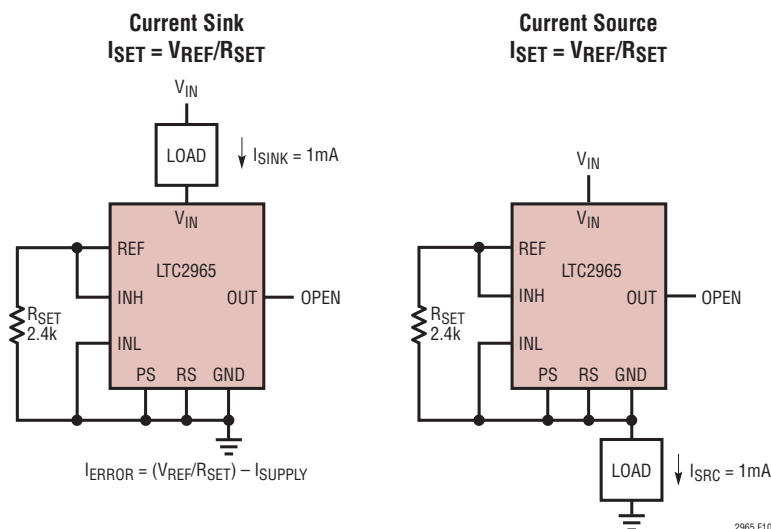$I_{SET} = V_{REF}/R_{SET}$

Figure 10. LTC2965 Configured as High Voltage Current Source

TYPICAL APPLICATIONS

Configure the current to be no greater than 1mA to ensure that the REF voltage stays within ±1% tolerance. Current values larger than 1mA exceed the REF buffer's load regulation capability and cause the REF voltage to drop out of regulation.
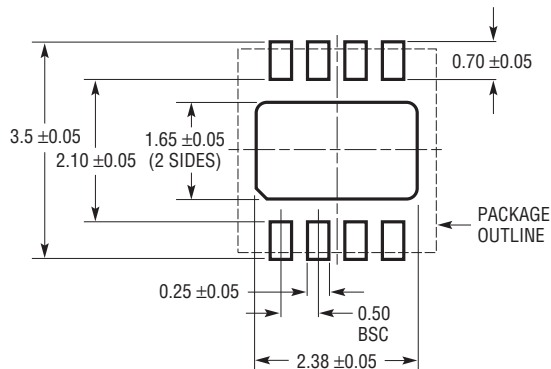
Shunt Mode Hysteretic Regulator

Figure 11 shows the LTC2965 used as the controller for a shunt mode hysteretic regulator to manage a battery-based solar power system. When the battery voltage reaches a lower float limit of 13.7V Q1 turns off and the solar panel current passes through to the battery and load. Once the battery voltage rises to the upper charging limit of 14.7V, Q1 turns on shorting the solar panel to ground with D1 isolating the battery from the shunt path. The upper and lower thresholds are generated from the on-chip reference as a separate external divider to set INH and INL and scaled by 10x. The charging thresholds are temperature compensated by an NTC thermistor over a 0°C to 50°C range.
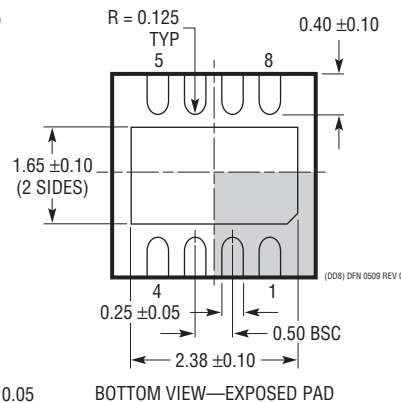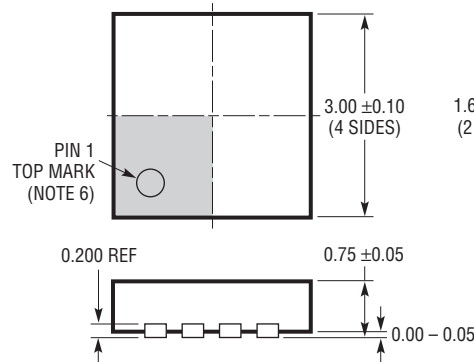
PACKAGE DESCRIPTION

Please refer to http://www.linear.com/product/LTC2965#packaging for the most recent package drawings.

DD Package
8-Lead Plastic DFN (3mm × 3mm)
(Reference LTC DWG # 05-08-1698 Rev C)

3.5 ±0.05

2.10 ±0.05

1.65 ±0.05
(2 SIDES)

0.70 ±0.05

PACKAGE
OUTLINE

0.25 ±0.05

0.50
BSC

2.38 ±0.05

RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS
APPLY SOLDER MASK TO AREAS THAT ARE NOT SOLDERED

3.00 ±0.10
(4 SIDES)

PIN 1
TOP MARK
(NOTE 6)

0.200 REF

0.75 ±0.05

0.00 – 0.05

R = 0.125
TYP

5

8

0.40 ±0.10

1.65 ±0.10
(2 SIDES)

(DD8) DFN 0509 REV C

4

1

0.25 ±0.05
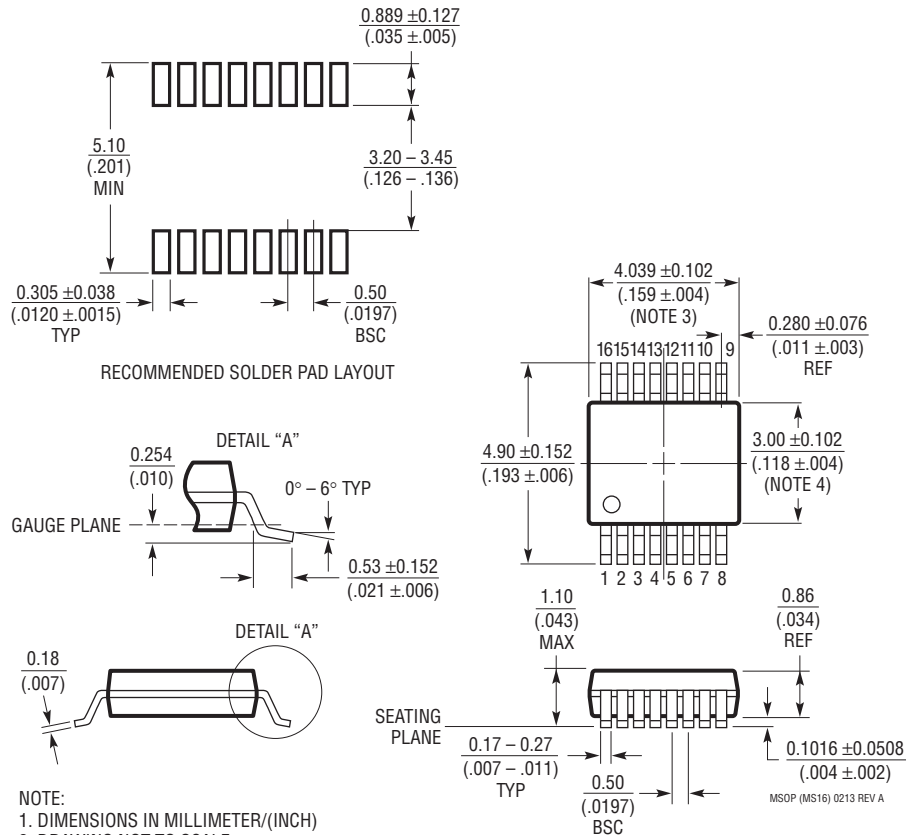
0.50 BSC

2.38 ±0.10

BOTTOM VIEW—EXPOSED PAD

NOTE:
1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE M0-229 VARIATION OF (WEED-1)
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE
   MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION
   ON TOP AND BOTTOM OF PACKAGE

PACKAGE DESCRIPTION

Please refer to http://www.linear.com/product/LTC2965#packaging for the most recent package drawings.

MS Package
16-Lead Plastic MSOP
(Reference LTC DWG # 05-08-1669 Rev A)

0.889 ±0.127
(.035 ±.005)

5.10
(.201)
MIN

3.20 – 3.45
(.126 – .136)

0.305 ±0.038
(.0120 ±.0015)
TYP

0.50
(.0197)
BSC

RECOMMENDED SOLDER PAD LAYOUT

DETAIL "A"

0.254
(.010)

0° – 6° TYP

GAUGE PLANE

0.53 ±0.152
(.021 ±.006)

DETAIL "A"

0.18
(.007)

4.039 ±0.102
(.159 ±.004)
(NOTE 3)

0.280 ±0.076
(.011 ±.003)
REF

16 15 14 13 12 11 10 9

4.90 ±0.152
(.193 ±.006)

3.00 ±0.102
(.118 ±.004)
(NOTE 4)

1 2 3 4 5 6 7 8

1.10
(.043)
MAX

0.86
(.034)
REF

SEATING
PLANE

0.17 – 0.27
(.007 – .011)
TYP

0.50
(.0197)
BSC

0.1016 ±0.0508
(.004 ±.002)

MSOP (MS16) 0213 REV A

NOTE:
1. DIMENSIONS IN MILLIMETER/(INCH)
2. DRAWING NOT TO SCALE
3. DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.
   MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
4. DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.
   INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
5. LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.102mm (.004") MAX

REVISION HISTORY

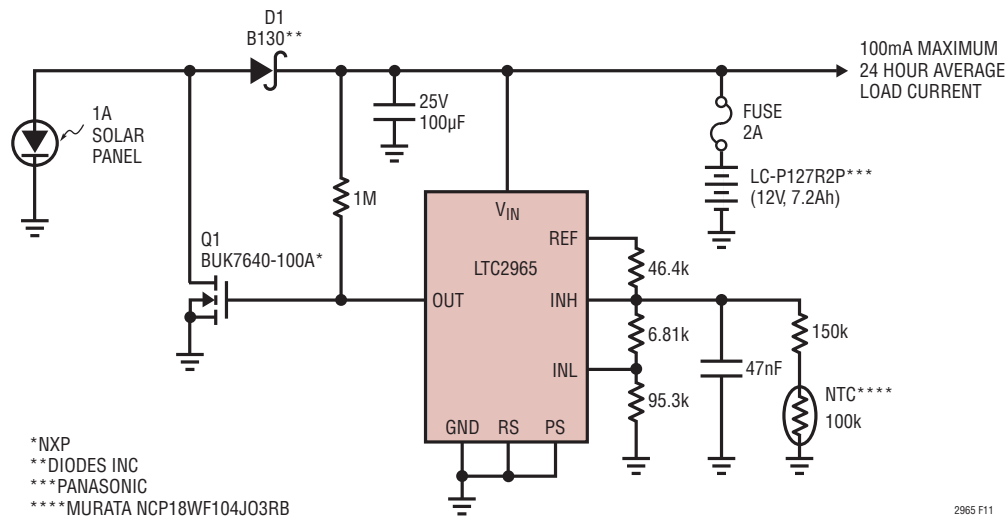| REV	DATE	DESCRIPTION	PAGE NUMBER
A	09/15	Fixed typos	3, 4, 10 – 12
B	03/16	Added Absolute Maximum Rating for INH and INL Pins	2
C	08/17	Corrected example error threshold calculations	10

TYPICAL APPLICATION

Figure 11. Shunt Mode Hysteretic Regulator

RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LTC1326	Micropower Triple Supply Monitor for 5V/2.5V, 3.3V and ADJ	4.725V, 3.118V, 1V Threshold (±0.75%) and ADJ
LTC1440/LTC1441/LTC1442	Ultralow Power Single/Dual Comparator with Reference	Adjustable Hysteresis, 3mm × 3mm × 0.75mm DFN Package
LTC1726/LTC1727/LTC1728	Micropower Triple Supply Monitor	Adjustable Reset and Watchdog Timeouts
LTC1985	Micropower Triple Supply Monitor with Push-Pull Reset Output	5-Lead SOT-23 Package
LTC2900/LTC2901/LTC2902	Programmable Quad Supply Monitor	Adjustable Reset, Watchdog Timer and Tolerance, 10-Lead MSOP and DFN Packages
LTC2903	Precision Quad Supply Monitor	6-Lead SOT-23 and DFN Packages
LTC2904/LTC2905 LTC2906/LTC2907	Three-State Programmable Precision Dual Supply Monitor	8-Lead SOT-23 and DFN Packages
LTC2908	Precision Six-Supply Monitor (Four Fixed and Two Adjustable)	8-Lead TSOT-23 and DFN Packages
LTC2909/LTC2919	Precision Triple/Dual Input UV, OV and Negative Voltage Monitor	Shunt Regulated V_{CC} Pin, Adjustable Threshold and Reset
LTC2910	Octal Positive/Negative Voltage Monitor	Separate V_{CC} Pin, Eight Inputs, Up to Two Negative Monitors Adjustable Reset Timer, 16-Lead SSOP and DFN Packages
LTC2912/LTC2913/LTC2914	Single/Dual/Quad UV and OV Voltage Monitors	Separate V_{CC} Pin, Adjustable Reset Timer
LTC2915/LTC2916 LTC2917/LTC2918	Single Voltage Supervisors with 27 Pin-Selectable Thresholds	Manual Reset and Watchdog Functions, 8- and 10-Lead TSOT-23, MSOP and DFN Packages
LTC2966	100V Micropower Dual Voltage Monitor	1.75V to 98V Monitoring Range, 3.5V to 100V Operating Range, 7µA Quiescent Current
LTC2960	36V Nano-Current Two Input Voltage Monitor	36V, 850nA Quiescent Current, 2mm × 2mm 8-Lead DFN and TSOT-23 Packages
LT6700	Micropower Dual Comparator with 400mV Reference	SOT-23, 2mm × 3mm DFN Package

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[LTC2965CMS#TRPBF](#)   [LTC2965IMS#TRPBF](#)